

## 酸化鐵還元에 대한 添加物の 効果

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(접수 1974. 1. 17)

## Effect of Additives on the Reduction of Hematite

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### 요 약

수소로 산화철을 환원시킬 때 환원속도에 미치는 첨가물의 효과와 역할을 규명하기 위하여 산화철의 중량감소, 격자정수, 전기전도도를 측정하였다. 그 결과  $\text{Li}_2\text{O}$ 는 환원속도와 전기전도도를 증가시켰고  $\text{Al}_2\text{O}_3$ 와  $\text{Ga}_2\text{O}_3$ 는 감소시켰는데,  $\alpha\text{-Fe}_2\text{O}_3$ 의 결손구조와 전자이동기구로서 이를 설명하였다.

한편  $280^\circ\sim 425^\circ\text{C}$ 의 실험범위에서  $\alpha\text{-Fe}_2\text{O}_3$ 는 금속철로 직접 환원되었으며, 모든 속도론적 Data는 Avrami 식에 잘 맞았다.

### Abstract

To clarify the effect of additives on the reduction rate of hematite with hydrogen and the role of additives, the loss of weight, the lattice constant, and the electrical conductivity have been measured for pure and doped hematite. The reduction rate was increased and the electrical conductivity was decreased by the addition of  $\text{Li}_2\text{O}$  and trivalent oxides ( $\text{Al}_2\text{O}_3$  and  $\text{Ga}_2\text{O}_3$ ). The effect of additives on the electrical conductivities is discussed in term of electron transfer mechanism. In the temperature range of  $280^\circ$  to  $425^\circ\text{C}$ , hematite is directly reduced to metallic iron. The kinetic data show good agreement with Avrami equation.

### I. Introduction

The investigation of the reduction of iron oxides with hydrogen has been studied by many investigators.

Their study was partly practical, dealing with reduction process, and partly theoretical, involving comprehensive laboratory experiments for the effect of temperature, pressure, gas composition and the shape of iron oxide on the reduction rate. Despite the numerous papers on

the reduction of iron oxide, a few papers concerning the additive or impurity effect on this important metallurgical and industrial processes were reported. Since Schenck and his coworkers<sup>1)</sup> suggested that the rate of reduction was accelerated when lime was added to wustite in 1929, some papers were reported on this very interesting process. Williams and Ragatz<sup>2)3)</sup> found that potassium and sodium carbonates increased the reduction rate of magnetite ore. McGeorge et al.<sup>4)</sup> found that the addition of  $\text{Na}_2\text{O}_3$  to the iron ore such as Cuban lateritic hematite and Cornwall dense magnetite increased the reduction rate and addition of  $\text{Na}_2\text{O}$  to chemical pure grade  $\text{Fe}_2\text{O}$  decreased the reduction rate with hydrogen. From this result they concluded that the additive, alkali oxides, apparently reacted with the impurities in ores freeing the iron oxide for reduction. Morawietz et al.<sup>5)</sup> recognized additional effect of iron powder and other metals such as nickel, cobalt and copper on the reduction of magnetite. Recently Khallafalla and Weston<sup>6)</sup> also studied additive effect of alkali and alkaline earth oxide on the reduction of wustite pellet with carbon monoxide at  $1000^\circ\text{C}$  and found that small amount of additive (below 0.69 atomic %) had a strong accelerating effect on the reduction rate of wustite to metallic iron. The extent of the reduction rate enhancement was proportional to ionic radius and electronic charge of the additives. On the other hand, Tigershold<sup>7)</sup>, Edstrom<sup>8)</sup> and Esche and Steinhauer<sup>9)</sup> reported the accelerating effect of calcium compound additives on the reduction rate of hematite or magnetite.

As mentioned above, although the addition of impurities to iron oxide accelerates the reduction rate, the role of additives on the reduction and the actual mechanism of the reduction process of iron oxides have not been clarified. The aim of the present work is to clarify the role of additives in the reduction of hematite based on the defective structure of hematite.

## II. Experimental

**Preparation of Sample:** Hematite was prepared from chemical pure grade ferrous oxide (99.9%). Ferrous oxide was oxidized for 4 hrs at  $700^\circ\text{C}$  in air and

quenched to room temperature in air. X-ray diffraction data of the resulting materials showed the same pattern as  $\alpha\text{-Fe}_2\text{O}_3$ . Lithium, aluminium and gallium nitrate were used as the additives. These additives were selected as their ionic radius are nearly equal to that of iron ion. Their ionic radius and other properties were shown in Table I and compared with that of hematite ( $\alpha\text{-Fe}_2\text{O}_3$ ).

Doping was made as follows: (1) A known weight of an additive was dissolved in distilled water, (2) a known weight of hematite was mixed with above additive solution, (3) the solution was completely dried with infrared lamp while being agitated continuously for about 1 hr, and the resulting agglomerate was pulverized, (4) the doped hematite was slowly heated from room temperature to the melting point of the additive and for 1 hr at temperature which is  $20^\circ\text{C}$  higher than melting point of the additive, and finally heated for 6 hrs at  $1000^\circ\text{C}$  in air followed by quenching to room temperature in air, (5) the resulting oxide was pulverized and then kept in a desiccator. Hematite sample was also heated for 6 hrs at  $1000^\circ\text{C}$  in air to make the same condition with all doping samples.

**X-ray Analysis:** Hematite and all doped samples were analyzed by the X-ray diffractometer (Holland Phillips PW-1051) for measuring the lattice constant and for the identification. X-ray operating conditions were: Target  $\text{CoK}\alpha$ ; filler Fe; voltage 30kV; current 10mA; counter G.C.; full scale counts 800 cps; scanning speed  $2^\circ 2\theta/\text{min}$  and angle range  $20\sim 80^\circ$ . In the measurements of lattice constants, scanning speed was one-fourth degree in  $2\theta$  per minute, time constant 4 sec and angle range from  $150_\theta$  to  $50^\circ$ . The reduction products were also analyzed.

**Electrical Conductivity:** Conductivities of all 0.5 atomic% doped sample and pure hematite were measured.<sup>10)</sup> The pellets with 10mm in diameter and about 5mm in length were used as samples of electrical conductivity.

**Other Measurements:** Surface area of all samples were measured by the B.E.T. method. The sizes of particle of all samples were measured and the shape of the samples and some reaction products were observed

with a electron microscope.

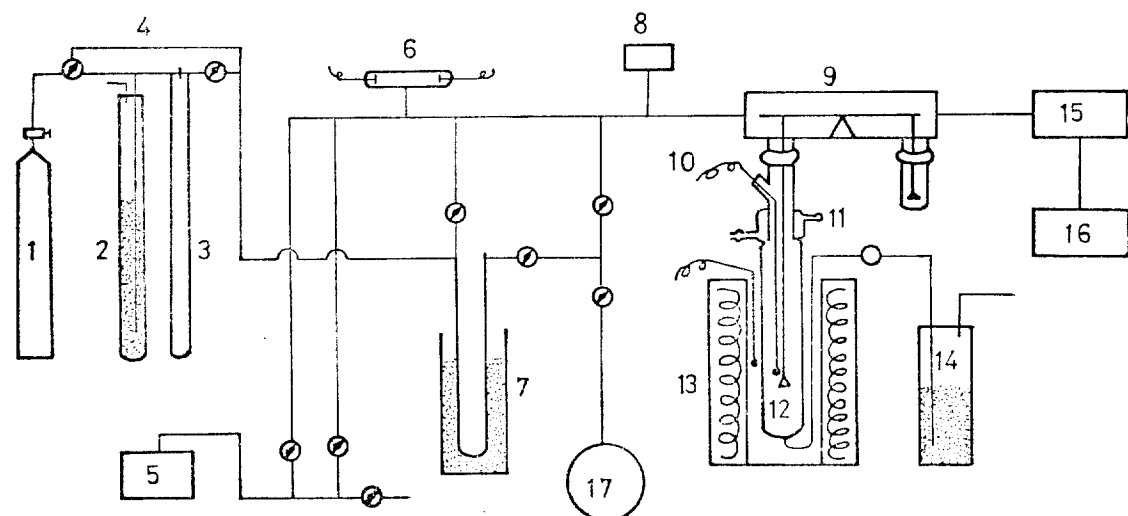
**Apparatus and Method:** The experimental apparatus as shown in Fig. 1 consists of four main parts: the gas flow control system, a vacuum line, the microbalance system, and the temperature control system. The hydrogen gas from the stock bomb is introduced to the top of reaction tube through the vacuum line and flow down around the platinum sample basket and flow out at the bottom. The size of the platinum sample basket is 15mm in diameter and 4mm in length. The flow rate of hydrogen was controlled by a reducing valve and measured with a calibrated venturi flow meter. Water in hydrogen was frozen out in a liquid nitrogen trap attached to the vacuum line. The gas left the system through the liquid paraffin trap which was attached to prevent the back flow of air. An electrical resistance furnace which is movable in vertical directions was fitted around the reaction tube. Temperature was automatically controlled by a Pt and Pt-13%Rd thermocouple located near the furnace wall and measured by the same type of thermocouple located just upper the sample basket.

The hydrogen gas was introduced into the reaction tube evacuated to  $10^{-3}$  torr at the desired temperature. An ionization gauge and a Pirani gauge used for

measuring the pressure. A loss-in-weight was measured by the Shimadzu Recording Micro-Balance (Type RMB 50V) and automatically recorded by the TOA Electronic Polyrecorder(model EPR 10A).

The experiments were carried out as follows: (1) a platinum sample basket containing the sample of 40 mg was suspended by a fine platinum wire attached to the top of the microbalance beam, (2) air in the quartz reaction tube was evacuated by a vacuum pump to about  $10^{-3}$  torr, (3) the quartz reaction tube was heated to the experimental temperature, (4) the hydrogen gas was introduced into the reaction tube and from that time the loss-in-weight was measured. When the reduction was finished, hydrogen gas in the reaction tube was evacuated to  $10^{-3}$  torr, quenched to room temperature, filled with high purity nitrogen to 1 atmosphere, and then stand for about 24 hrs. The products were used for X-ray analysis and electro-microscopic observation.

The range of experimental temperature were from 280° to 425°C. The influence of hydrogen flow rate on the reduction rate was checked at 300°C. As shown in Fig.2 there is no influence of the flow rate of hydrogen on the reduction rate beyond the flow rate of 57 cc/min. Therefore, this experiment was performed



1. hydrogen bomb 2. water cylinder for flow rate control 3. venturi manometer 4. by-pass line 5. rotary pump  
6. ionized gauge 7. liquid nitrogen trap 8. Pirani gauge 9. micro-balance(Shimadzu RMB-50V) 10. Pt-Pt-13%Rd thermocouple  
11. water condenser 12. platinum sample basket 13. electrical furnace 14. liquid paraffin trap 15. controller of balance  
(Shimadzu RMB-50V) 16. electronic polyrecorder (TOA EPR-10A) 17. N<sub>2</sub> gas

Fig.1 Schematic Diagram of Experimental Apparatus

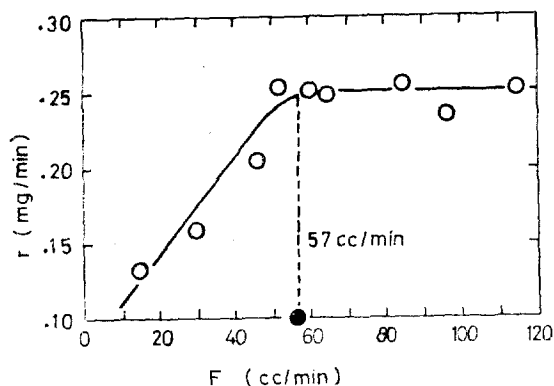


Fig. 2 Influence of the Flow rate of Hydrogen on the Reduction Rate of Pure Hematite at 300°C

at constant flow rate of 57 cc/min which corresponds to a linear gas velocity of 0.1 cm/sec in the reaction tube.

### III. Results

The physical properties of the pure and doped hematite are given in Table 1. The particle size distribution of the pure and doped hematite ranges from 0.47 to about 4 $\mu$  and from 0.94 to 3.14 $\mu$ , respectively. Surface area was 0.74m<sup>2</sup>/gr for pure hematite and 1~0.5m<sup>2</sup>/gr for all doped samples. The surface area of 0.7~1.0 m<sup>2</sup>/gr for doped and pure hematite was very small in comparison with 10m<sup>2</sup>/gr for the natural hematite. Lattice constant in Å unit as a function of additive contents is shown for three doped samples in 280° to

Fig. 3. The lattice constant obviously decreases with increasing contents of additive except for that of pure hematite. With this exception, the trend of curves agrees with Vegard rule<sup>16)</sup> stating that the lattice parameter of solid solution linearly increases or decreases with the content of a constituent component. For the system of Fe<sub>2</sub>O<sub>3</sub>-Li<sub>2</sub>O,  $\alpha$ -lithium ferrite (LiFe<sub>2</sub>O<sub>4</sub>) was found from the X-ray diffraction data. For Al<sub>2</sub>O<sub>3</sub> and Ga<sub>2</sub>O<sub>3</sub> doped samples, no compound formation was observed.<sup>18)</sup>

The fraction of reaction( $\alpha$ )-time curves are sigmoidal having the induction time of relatively long duration. The time decreased with the increasing temperature and the addition of time. The induction time ( $t_0$ ) and corrected 50% reduction time are shown in Table 2. The corrected 50% reduction time ( $t_{0.5R}$ ) was defined as follows;  $t_{0.5R} = t_{0.5} - t_0$  where  $t_{0.5}$  is the time which is necessary for the 50% reduction. The result for Li<sub>2</sub>O doped sample is given in Fig. 4. The effects of the reaction and 50% reduction time at above 340°C were small and those under 340°C were very large. are shown in Fig. 5 for pure and 0.5% doped samples. Fig. 6 show the effect of additive contents at 380°C. All of the reduction data in the temperature range of 425°C are expressed with Avrami equation<sup>11) 12)</sup> that was derived under the assumption of the phase boundary controlled reaction. The results are shown in from Fig. 7 to Fig. 9 and the rate constant calculated

Table. 1 The Physical Properties of the Pure and Doped Hematite, and the Additives

Properties	Additive Additive Content(at. %)			Li <sub>2</sub> O			Al <sub>2</sub> O <sub>3</sub>			Ga <sub>2</sub> O <sub>3</sub>			Hematite $\alpha$ -Fe <sub>2</sub> O <sub>3</sub>
	0.5	1.0	2.0	0.5	1.0	2.0	0.5	1.0	2.0	0.5	1.0	2.0	
Particle Size ( $\mu$ )	0.47 -3.93	0.47 -4.40	0.47 -4.04	0.47 -4.40	0.47 -4.04	0.47 -4.04	0.47 -3.39	0.47 -3.14	0.47 -4.40	0.94~3.14			
Surface Area (m <sup>2</sup> /gr)	0.91	0.70	0.44	0.97	0.99	0.77	0.99	0.75	1.17	0.74			
Lattice Constant (Å)	5.4251	5.4230	5.4228	5.4176	5.4239	5.4204	5.4239	5.4237	5.4240	5.4228			
Activation Energy (kcal/mole)	15.15	16.18	16.43	19.65	19.27	18.90	19.03	20.56	21.67	16.08			
Solid Solution	LiFe <sub>2</sub> O <sub>4</sub>			none			none						
Ionic Radius (Å)	Li <sup>1+</sup> 0.61			Al <sup>3+</sup> 0.57			Ga <sup>3+</sup> 0.62			Fe <sup>3+</sup> 0.67			
System	Cubic			Trigonal			Rhombohedral			Rhombohedral			
Original Form	LiNO <sub>3</sub>			Al(NO <sub>3</sub> ) <sub>3</sub> 9H <sub>2</sub> O			Ga(NO <sub>3</sub> ) <sub>3</sub> 8H <sub>2</sub> O						
Melting Point (°C)	261			73			110			1560			
Molecular Weight	68.95			375.15			399.87			159.70			

Table 2. Induction Time ( $t_0$ ) and Corrected 50% Reduction Time ( $t_{0.5R}$ ) in Minutes

Additives		Li <sub>2</sub> O			Al <sub>2</sub> O <sub>3</sub>			Ga <sub>2</sub> O <sub>3</sub>			α-Fe <sub>2</sub> O <sub>3</sub>
Additive Contents (atomic %)		0.5	1.0	2.0	0.5	1.0	2.0	0.5	1.0	2.0	
Temp°C											
280	t <sub>0</sub>	24	28	30	90	70	50				20
	t <sub>0.5R</sub>	174	93	92	190	167	160				52
300	t <sub>0</sub>	8.5	14.5	17.0	10.0	36.0	32.0	40.0	80.0	110.0	15
	t <sub>0.5R</sub>	36.5	41.5	58.0	113.0	94.0	93.0	114.0	160.0	?	51.0
320	t <sub>0</sub>							30.0	50.0	60.0	12.0
	t <sub>0.5R</sub>							62.0	83.0	152.0	43.0
340	t <sub>0</sub>	6.6	7.7	8.0	15.0	10.0	4.0	8.3	15.0	20.0	8.0
	t <sub>0.5R</sub>	17.1	23.3	27.3	37.0	39.0	34.0	44.7	44.0	62.0	24.0
380	t <sub>0</sub>	0.0	0.0	0.0	3.3	0.5	0.5	5.0	7.0	10.0	2.5
	t <sub>0.5R</sub>	8.0	8.3	9.3	10.5	13.5	10.5	22.0	20.0	25.0	8.5
400	t <sub>0</sub>	0.0	0.0	0.0	2.0	0.3	0.0	1.0	1.0	3.0	1.6
	t <sub>0.5R</sub>	6.0	5.3	6.3	14.0	9.7	6.0	11.0		20.0	7.9
425	t <sub>0</sub>	0.0	0.0	0.0	1.0	0.0	0.0	0.0	0.0	3.0	0.0
	t <sub>0.5R</sub>	3.8	0.0	4.3	11.0	6.0	3.0	4.0	6.0	15.0	4.0

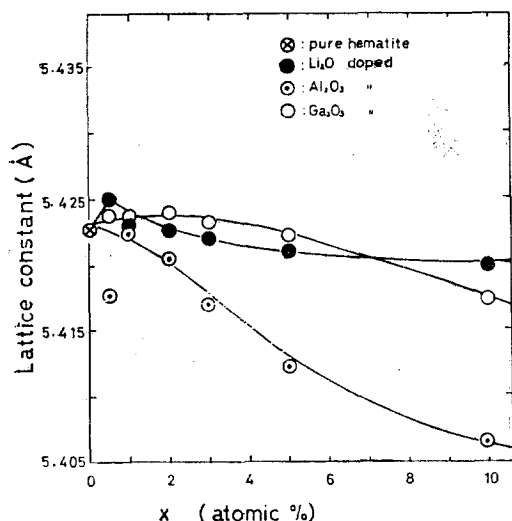
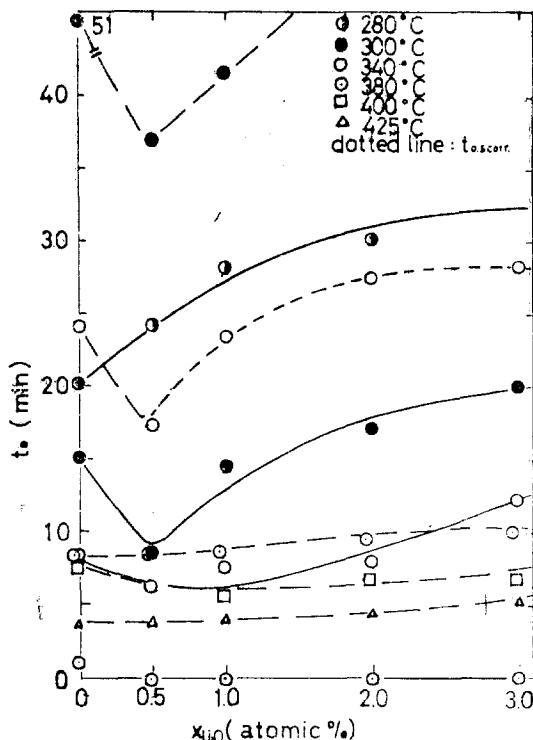


Fig. 3 Change of Lattice Constant of Sample with Dopant Contents

from Avrami plot are plotted against  $1/T$  in Fig. 10, 11 and 13.

Table 1 shows the activation energies for each samples (in the temperature range of 280° to 425°C) calculated from Arrhenius plot. The energies of activation for pure hematite are 16.1 kcal/mole. This value is the same with 15.3 kcal/mole by McGeorge,<sup>4)</sup> 16.57 kcal/mole by Feinman<sup>13)</sup> and 15.45 kcal/mole Mckewan<sup>14)</sup> measured at the same temperature ranges. In these figures, the reductivity of samples obviously decreases with increasing the dopant contents except

Fig. 4 Relation between Dopant Content on Induction Time ( $t_0$ ) and corrected 50% Reduction Time at Various Temperature

$Al_2O_3$  doped sample. For  $Al_2O_3$  doped sample, the reductivity decreases by doping, however, the quantitative effect of the additive contents was not obvious. The rate constants obtained at 300°C and 400°C are

plotted a function of the additive contents in Fig. 13. The rate constants of  $\text{Li}_2\text{O}$  and  $\text{Ga}_2\text{O}_3$  doped samples decrease with increasing the additive contents and in the case of  $\text{Al}_2\text{O}_3$  increases with additive content up to 2.0 atomic%. All the results obtained

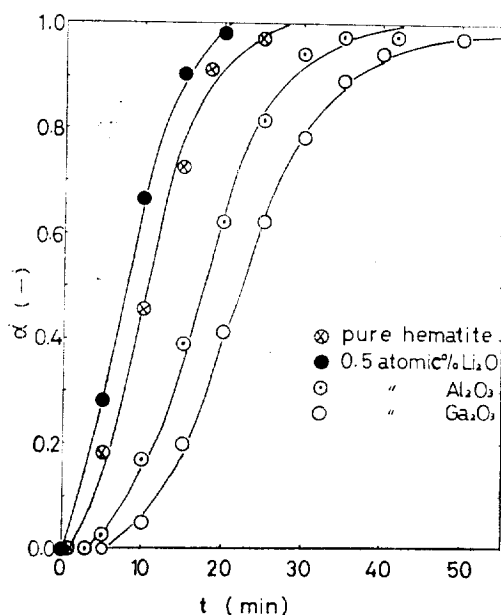


Fig. 5 Effect of Dopants on the Reduction of Hematite at 380°C

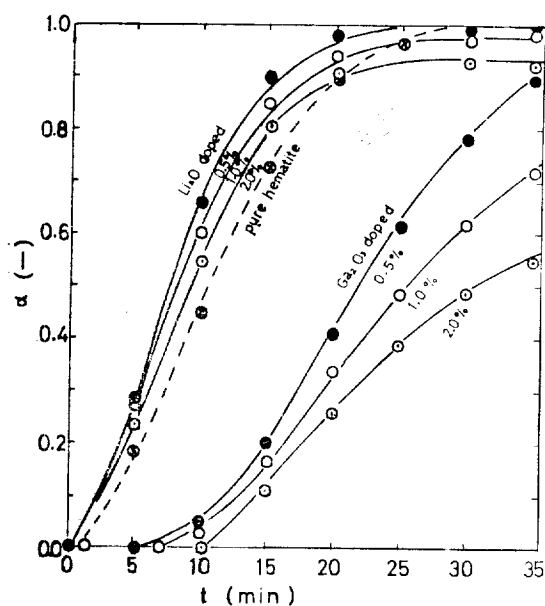


Fig. 6 Effects of Dopants and Their Content on the Reduction of Hematite at 380°C

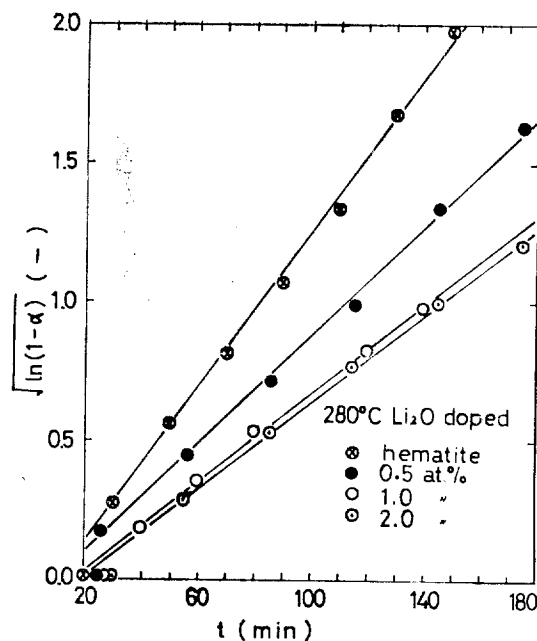


Fig. 7 Avrami Plot for  $\text{Li}_2\text{O}$  Doped Hematite at 280°C

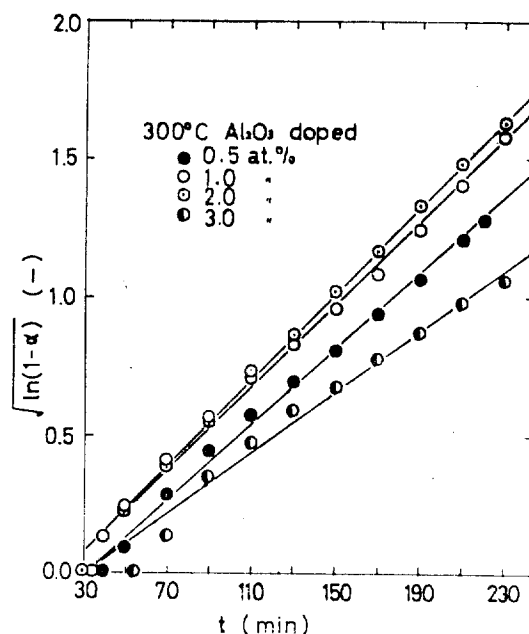


Fig. 8 Avrami Plot for  $\text{Al}_2\text{O}_3$  Doped Hematite at 300°C

for three additives can not be shown in Fig. 14, however, the trend is the same in all temperature range.

For the understanding of the reduction processes, the

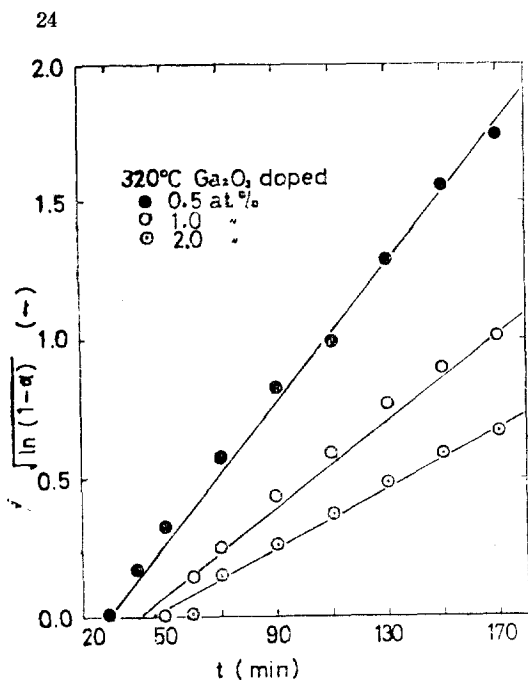


Fig. 9 Avrami Plot for  $\text{Ga}_2\text{O}_3$  Doped Hematite at  $320^\circ\text{C}$

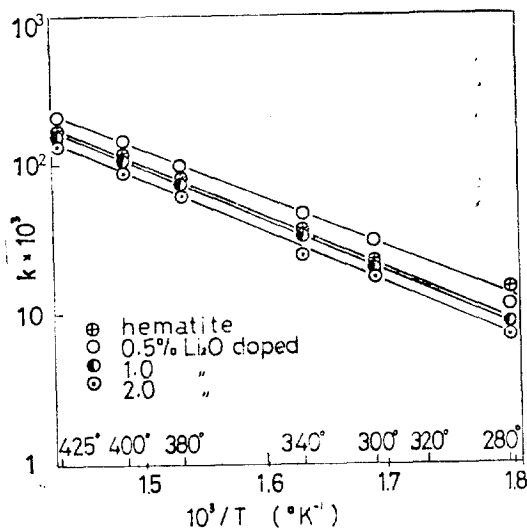


Fig. 10 Temperature Dependence of Pure and  $\text{Li}_2\text{O}$  Doped Hematite

reduction was stopped by quenching at various stages and after letting it stand for 24 hrs in nitrogen gas. The product was analyzed with X-ray. All the X-ray diffraction data revealed that the product was composed of magnetite and metallic iron. This result represents that the hematite was directly converted to metallic

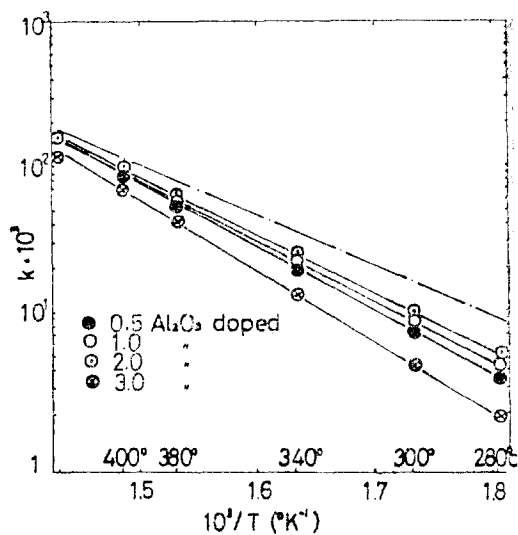


Fig. 11 Temperature Dependence of the Rate Constant of pure- and  $\text{Al}_2\text{O}_3$  Doped Hematite

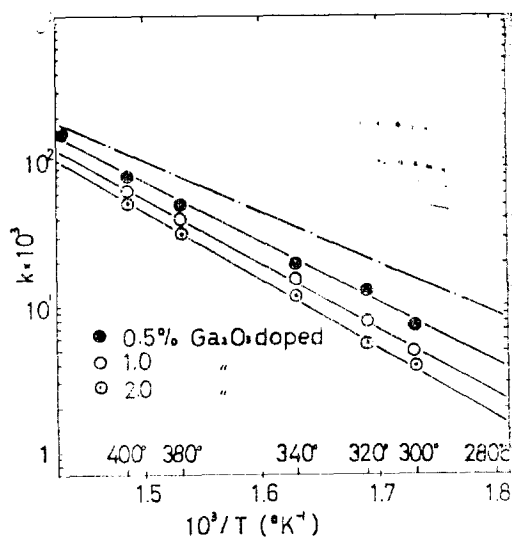


Fig. 12 Temperature Dependence of the Rate Constant of Pure and  $\text{Ga}_2\text{O}_3$  Doped Hematite

iron without passing through other intermediates such as magnetite, wustite and other complex compounds.

Finally, in order to clarify the structure of doped samples and the role of the dopants in the reduction, the electrical conductivities of 0.5 atomic % doped samples and pure hematite were measured under  $2.2 \times 10^{-3}$  torr and shown as a function of reciprocal temperature in Fig. 14. The electrical conductivity of the

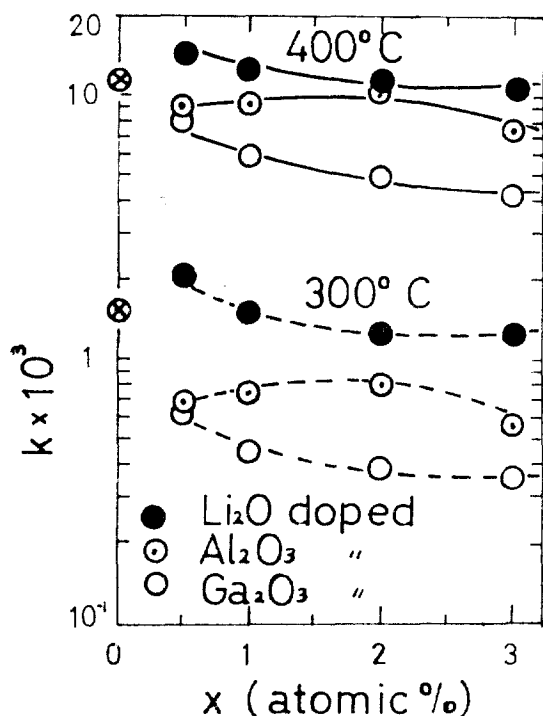


Fig. 13 Effect of Dopant Contents on the Reduction Rate at 300° and 400°C

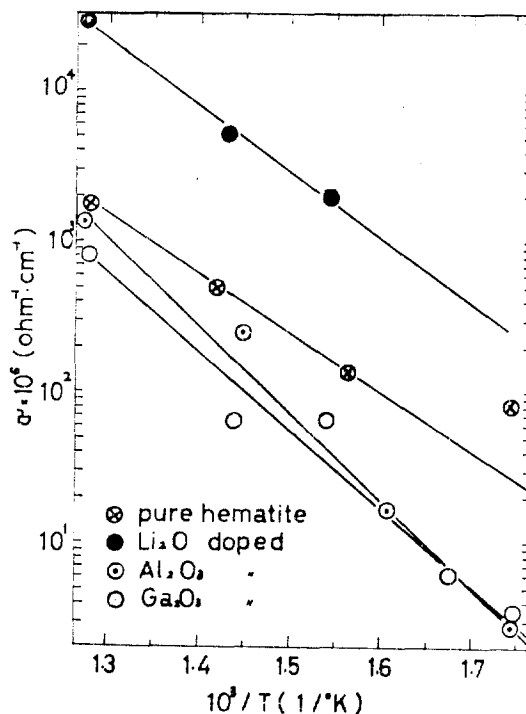


Fig. 14 Temperature Dependence of Electrical Conductivity of Pure and Doped Hematite at  $2.2 \times 10^3$  torr in Air.

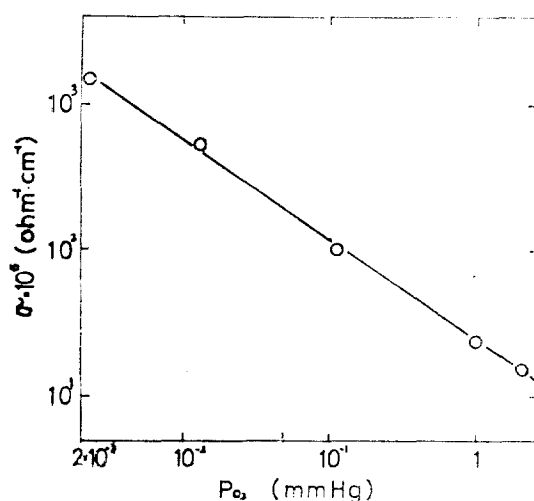


Fig. 15 Electrical Conductivity of Pure Hematite as a Function of Oxygen partial Pressure at 515°C

$\text{Li}_2\text{O}$  doped sample was approximately tenfold greater than that of pure hematite and those of  $\text{Al}_2\text{O}_3$  and

$\text{Ga}_2\text{O}_3$  doped sample were about one-fifths throughout the temperature ranges studied. Fig. 15 shows the electrical conductivities of pure hematite as a function of oxygen partial pressure at the constant temperature of 515°C. The conductivity decrease quickly at initial stage and slowly at more than 2 hrs. Therefore, the measurement was made at 2 hrs. The electrical conductivity decreases with increasing the oxygen partial pressure. This result suggests that hematite used is a n-type semiconductor.

### Discussion

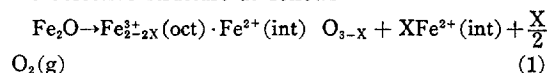
The difference in the reactivity of the samples may be ascribed to the difference in the defective structure of hematite. Hematite ( $\alpha\text{-Fe}_2\text{O}_3$ ) is rhombohedral crystal with the lattice constant of  $a=5.4228 \text{ \AA}$  and  $x=55.17^\circ$ . The  $\text{O}^{2-}$  ions are arranged in a close-packed hexagonal lattice and two-thirds of the octahedral interstices are occupied by  $\text{Fe}^{3+}$  ions. This oxide has



a small oxygen deficit and iron ions is probably in additional interstitial positions. Tannhauser<sup>15)</sup> suggested the existence of interstitial  $\text{Fe}^{2+}$  ion. Whereas the electrical conductivity plotted against oxygen partial pressure in Fig. 15 suggests that hematite is possibly n-type semiconductor. However, the effect of dopants ( $\text{Li}_2\text{O}$ ,  $\text{Al}_2\text{O}_3$  and  $\text{Ga}_2\text{O}_3$ ) in the electrical conductivity suggests that hematite is p-type. No agreement between both results was obtained.

Tannhauser<sup>15)</sup> proposed that the mechanism of the conductivity in hematite is the electron transfer between  $\text{Fe}^{3+}$  and  $\text{Fe}^{2+}$  ions in the octahedral position. The  $\text{Fe}^{2+}$  ions in hematite are incorporated by the oxygen deficit and considered to be located at the interstitial positions. However, no definite structure is given.

With these considerations concerning the defective structure of hematite, the authors tentatively assume the defective structure as follows:



Equation (1) states that each half of  $\text{Fe}^{2+}$  ions occupies the octahedral and the interstitial positions. The assumption of the equal distribution of  $\text{Fe}^{2+}$  ions will not change essentially the character of foregoing discussions. From equation (1), the concentration of  $[\text{Fe}^{2+}(\text{int})]$  is obtained to be proportional to  $\text{Po}_2^{-1/2}$  and equal to that of  $[\text{Fe}^{2+}(\text{oct})]$ . The conductivity by the electron transfer is proportional to the product  $[\text{Fe}^{3+}(\text{oct})] \cdot [\text{Fe}^{2+}(\text{int})]$  and  $[\text{Fe}^{3+}(\text{oct})] \rightarrow [\text{Fe}^{2+}(\text{oct})]$ . Thus, the conductivity is expected to be proportional to  $[\text{Fe}^{2+}(\text{int})]$  and to  $\text{Po}_2^{-1/2}$ . The pressure dependency of the conductivity was proportional to  $\text{Po}_2^{-1/4}$  and the discrepancy between the theoretical and experimental is not so large in view of the rough assumption made previously.

If dopant  $\text{Li}_2\text{O}$  incorporated in hematite substitutes the interstitial  $\text{Fe}^{2+}$  ion expelling the  $\text{Fe}^{2+}$  ions to the octahedral position, the probability of the electron transfer will increase and the conductivity is expected to increase. If trivalent metallic ions ( $\text{Al}^{3+}$  and  $\text{Ga}^{3+}$ ) incorporated occupy the octahedral, the probability of the electron transfer decrease and the low conductivity of  $\text{Al}^{3+}$  and  $\text{Ga}^{3+}$  doped samples is reasonable. Further study on the distribution of the doped ions will be

done to verify the above discussion.

As for the reactivity of doped hematite, the elucidation of the effect of dopants seems to be more difficult because the detailed defect structure of hematite is not clear. The increase of  $\text{Fe}^{3+}$  ion in the octahedral position due to the incorporation of  $\text{Al}_2\text{O}_3$  and  $\text{Ga}_2\text{O}_3$  seems to result the more stoichiometric composition than pure hematite. The more stoichiometric compound is expected to have the less reducibility.  $\text{Li}_2\text{O}$  doped hematite may be considered to have the more defective than pure hematite and therefore, to have the high reactivity.

The alternative elucidation for  $\text{Li}_2\text{O}$  doped sample have to be discussed here. Roy and et al.<sup>17)</sup> have presented the phase diagram of  $\text{Fe}_2\text{O}_3$ - $\text{Li}_2\text{O}$  system. The phase diagram states that  $\text{Li}_2\text{O}$  makes no solid solution with hematite and only lithium ferrite coexisting with hematite as a mixture. Therefore, lithium ferrite particles are thought to be dispersed homogeneously in hematite. The texture seems to increase the reactivity of doped hematite. The dispersed ferrite may retard the mutual sintering of iron particles and hold a good condition for further progress of the reaction.

## Conclusion

1. In the temperature range of  $280^\circ$  to  $425^\circ\text{C}$  hematite directly change to metallic iron.
2. The kinetic data for the reduction of pure and doped hematite are successfully expressed by Avrami equation.
3. The reduction rate increases and the electrical conductivity decreases for the  $\text{Li}_2\text{O}$  and trivalent oxides ( $\text{Al}_2\text{O}_3$  and  $\text{Ga}_2\text{O}_3$ ) studied.
4. The effect of dopants on the electrical conductivity is discussed with the electron transfer mechanism.

## Acknowledgments

This investigation was carried out at the Komatsu Laboratory, Department of Chemical Engineering, Tokyo Institute of Technology, by the fund of

Japanese National Commission For UNESCO. The author thanks all collaborators at Komatsu Laboratory and UNESCO office for valuable help with investigations. For advice on the X-ray investigations the author is indebted to professor Kato and his laboratory members. The author's thanks are especially due to Dr. Professor W. Komatsu and Dr. Y. Moriyoshi, who have given extremely valuable aid and fruitful discussions during the work.

### Nomenclature

$F$ ; flow rate of hydrogen [cc/min]  
 $P$ ; partial pressure of oxygen [mmHg]  
 $r$ ; rate of loss-in-weight [mg-O<sub>2</sub>/min]  
 $t = t_{\text{corr}} + t_0$ ; reduction time [min]  
 $t_{\text{corr}}$ ; corrected reduction time [min]  
 $t_0$ ; induction time [min]  
 $t_{0.5}$ ; 50% reduction time [min]  
 $t_{0.5\text{corr}}$ ; corrected 50% reduction time [min]  
 $w$ ; oxygen weight of hematite after reduction [mg]  
 $w_0$ ; initial oxygen weight of hematite [mg]  
 $x$ ; content of additive [atomic %]  
 $x_{\text{Li}_2\text{O}}$ ; content of Li<sub>2</sub>O-additive [atomic %]  
 $\alpha = (w_0 - w)/w_0$ ; fractional conversion [—]  
 $\delta$ ; electrical conductivity [1/ohm cm]

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