

## Chemical absorption of carbon dioxide into oxirane solution containing ID-CP-MS41 catalyst

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**Abstract**—CP-MS41 was synthesized by hydrolysis of tetraorthosilicate, as a silicon source, with 3-chloropropyltriethoxysilane as an organosilane using cetyltrimethylammonium bromide as a template. ID-CP-MS41 was synthesized by immobilization of imidazole on the CP-MS41 and was dispersed in organic liquid as a mesoporous catalyst for the reaction between carbon dioxide and oxirane. Phenyl glycidyl ether and glycidyl methacrylate were used as oxiranes. Carbon dioxide was absorbed into the oxirane solution in a stirred batch tank with a planar gas-liquid interface within a range of 0–2.0 kmol/m<sup>3</sup> of oxirane and 333–363 K at 101.3 kPa. The measured values of absorption rate were analyzed to obtain the reaction kinetics using the mass transfer mechanism associated with the chemical reactions based on the film theory. The overall reaction of CO<sub>2</sub> with oxirane, which is assumed to consist of two steps—i) a reversible reaction between oxirane (B) and catalyst of ID-CP-MS41 (QX) to form an intermediate complex (C<sub>1</sub>), and ii) irreversible reaction between C<sub>1</sub> and CO<sub>2</sub> to form QX and five-membered cyclic carbonate (C)—was used to obtain the reaction kinetics through the pseudo-first-order reaction model. Polar solvents such as *N*, *N*-dimethylacetamide, *N*-methyl-2-pyrrolidinone, and dimethyl sulfoxide affected the reaction rate constants.

Key words: Absorption, Carbon Dioxide, Oxirane, Imidazole, MCM-41

### INTRODUCTION

The chemical fixation of carbon dioxide has become an important research topic because of the danger posed by global warming, and conversion of carbon dioxide into valuable substances is an extremely attractive solution. The reaction of CO<sub>2</sub> with oxiranes leading to 5-membered cyclic carbonates is well known [1], and these product carbonates can be used as polar aprotic solvents, electrolytes for batteries, and sources of reactive polymers [2]. The synthesis of cyclic carbonates by the reaction of CO<sub>2</sub> with oxirane has been performed using Lewis acids, transition metal complexes, and organometallic compounds as catalysts at high pressures, 10–50 atmospheres [3,4]. Milder conditions, however, atmospheric pressure in the presence of metal halides or quaternary onium salts, have been reported [5–10].

Research on oxirane-CO<sub>2</sub> reactions has focused on the reaction mechanism, the overall reaction kinetics, and the effect of the catalyst on the conversion [3–9]. Diffusion may affect the reaction kinetics in the mass transfer associated with the chemical reactions [11], so this effect is important to investigate the reaction kinetics of the gas-liquid heterogeneous reaction between CO<sub>2</sub> and oxirane. The kinetics of the reaction between CO<sub>2</sub> and oxiranes, such as phenyl glycidyl ether (PGE) and glycidyl methacrylate, have been studied using catalysts such as quaternary onium salts [12–15], polymer-supported catalyst with trialkylamine [16,17], and ionic liquid-supported catalyst with trialkylamine [18]. The reaction rate constants

were obtained using the measured absorption rate of CO<sub>2</sub>, analyzed with the mass transfer mechanism associated with the chemical reactions.

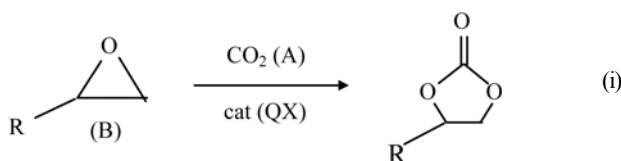
Various functionalized catalysts such as polymers, amorphous, and fumed silica have mild activity due to the low accessibility caused by the low/non porosity. However, the discovery of the M41S family [19] generated a great deal of interest in the synthesis of organically functionalized, mesoporous materials for application in the fields of catalysis, sensing, and adsorption, based on their high surface areas and large ordered pores ranging from 20 to 100 Å [20] with narrow size distributions. Their high chemical and thermal stabilities are also promising for the reactions of bulky substrate molecules. In general, hybrid organic-inorganic materials have been prepared *via* post-grafting or co-condensation techniques. In 2000, a grafting technique was developed through a co-condensation method for hybrid MCM-41 using halogenated organosilanes [21]. Recently, a new synthetic approach has been developed for the preparation of hybrid inorganic-organic mesoporous materials based on the co-condensation of siloxane and organosiloxane precursors in the presence of different templating surfactant solutions [22]. Also, a new grafting technique was described for the synthesis of hybrid MCM-41 and trialkylamine-immobilized ionic liquids containing high catalytic activity for the synthesis of cyclic carbonates [23].

In this study, PGE or GMA and the mesoporous particle, ID-CP-MS41 [16], of imidazole-immobilized ionic liquid on hybrid MCM-41 were used as the reactant and catalyst in the reaction between CO<sub>2</sub> and oxirane, respectively, to investigate the absorption kinetics of CO<sub>2</sub> with a diffusion model, which is one of the series of works to investigate the capture and utilization of carbon dioxide.

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## THEORY

To determine the reaction kinetics between an oxirane and carbon dioxide using ID-CP-MS41 (QX) containing ionic liquid of imidazole, it is necessary to understand the reaction mechanism in a heterogeneous reaction. Although the reaction mechanism shown in Eq. (i) is assumed for homogeneous [3,6-9] and heterogeneous [17] oxirane-CO<sub>2</sub> reactions, no reliable evidence has yet been reported. The rate-determining step is the attack of the anionic portion of the catalyst on the oxirane. The importance of this portion of the catalyst can be explained by this mechanism, whereby the overall reaction between CO<sub>2</sub> and oxirane to form the 5-membered cyclic carbonate is as follows:



where R is a functional group of -CH<sub>2</sub>-O-C<sub>6</sub>H<sub>5</sub> of PGE, or -CH<sub>2</sub>-O-C(=O)-C(CH<sub>3</sub>)=CH<sub>2</sub> of GMA, respectively. The overall reaction of (i) in this study is assumed to consist of two steps: i) a reversible reaction between oxirane (B) and ID-MS41 (QX) to form an intermediate complex (C<sub>1</sub>) and ii) irreversible reaction between C<sub>1</sub> and carbon dioxide (A) to form QX and the five-membered cyclic carbonate (C):



The reaction rate of CO<sub>2</sub> under the condition of a steady-state approximation to form C<sub>1</sub> is presented as follows:

$$r_A = \frac{C_B S_t}{\frac{1}{k_1} + \frac{1}{K_1 k_3 C_A} + \frac{C_B}{k_3 C_A}} \quad (1)$$

If the value of k<sub>1</sub> is very large, such that 1/k<sub>1</sub> approaches 0, Eq. (1) is arranged to

$$r_A = \frac{C_A C_B S_t}{\frac{1}{K_1 k_3} + \frac{C_B}{k_3}} \quad (2)$$

Under the assumptions that B is a nonvolatile solute, the gas phase resistance to absorption is negligible by using pure CO<sub>2</sub>, and thus Raoult's law applied. The mass balances of species A and B, using film theory accompanied by chemical reactions, and boundary conditions are given as follows:

$$D_A \frac{d^2 C_A}{dz^2} = r_A \quad (3)$$

$$D_B \frac{d^2 C_B}{dz^2} = r_A \quad (4)$$

$$z=0; \quad C_A = C_{Ai}; \quad \frac{dC_B}{dz} = 0 \quad (5)$$

$$z=L; \quad C_A = C_{AL}; \quad C_B = C_{Bo} \quad (6)$$

If the diffusion rate of CO<sub>2</sub> is not smaller than the reaction rate,

and the amount of dissolved CO<sub>2</sub> that reacts in the diffusion film adjacent to the phase boundary is negligible, compared to the CO<sub>2</sub> which reaches the bulk liquid phase in the unreacted state, the concentration of A in the bulk liquid phase is a finite quantity (C<sub>AL</sub>) and can be obtained from the following equation [11]:

$$k_L a_v (C_{Ai} - C_{AL}) = \frac{C_{AL} C_{Bo} S_t}{\frac{1}{K_1 k_3} + \frac{C_{Bo}}{k_3}} \quad (7)$$

In the general case that the reaction rate is given by Eq. (2), the material balance equations of component A and B based on the film theory, and the boundary conditions are put into the dimensionless form as follows:

$$\frac{d^2 a}{dx^2} = \frac{Mab}{1 + \alpha b} \quad (8)$$

$$\frac{d^2 b}{dx^2} = \frac{r q M a b^2}{1 + \alpha b} \quad (9)$$

$$x=0, \quad a=1, \quad \frac{db}{dx} = 0 \quad (10)$$

$$x=1, \quad a=a_L, \quad b=1 \quad (11)$$

where  $a = C_A/C_{Ai}$ ,  $b = C_B/C_{Bo}$ ,  $x = z/L$ ,  $r = D_A/D_B$ ,  $q = C_{Ai}/C_{Bo}$ ,  $K_1 = k_1/k_2$ ,  $\alpha = K_1 C_{Bo}$ ,  $M = \alpha k_3 D_A S_t / k_L^2$ ,  $k_L = D_A/L$ .

The enhancement factor of CO<sub>2</sub> ( $\beta$ ), defined as the ratio of the flux of CO<sub>2</sub> with chemical reaction to that without chemical reaction, is resented as follows:

$$\beta = - \left. \frac{da}{dx} \right|_{x=0} \quad (12)$$

At an initial absorption of CO<sub>2</sub>, stating that C<sub>B</sub> in the liquid film is constant as C<sub>Bo</sub>, the reaction rate constants, K<sub>1</sub> and k<sub>3</sub>, are obtained as follows;

Eq. (2) for the reaction between A and B is arranged as

$$r_A = k_o C_A \quad (13)$$

where k<sub>o</sub> is the pseudo-first-order reaction rate constant.

The mass balance of species A with the film theory accompanied by a pseudo-first-order reaction is given as follows:

$$D_A \frac{d^2 C_A}{dz^2} = k_o C_A \quad (14)$$

From the exact solution of Eq. (14),  $\beta$  can be derived as follows:

$$\beta = \left. \frac{da}{dx} \right|_{x=0} = \frac{Ha}{\tanh Ha} \quad (15)$$

where Ha is the Hatta number,  $\sqrt{k_o D_A / k_L}$ .

The following equation, derived from Eq. (2) and (13), is used to obtain k<sub>3</sub> and K<sub>1</sub>.

$$\frac{C_{Bo} S_t}{k_o} = \frac{1}{K_1 k_3} + \frac{C_{Bo}}{k_3} \quad (16)$$

## EXPERIMENTAL

### 1. Chemicals

All chemicals were of reagent grade and were used without fur-

**Table 1. Experimental data of absorption rate in the CO<sub>2</sub>/PGE and CO<sub>2</sub>/GMA system**

Solvent	$C_{Bo}$ (kmol/m <sup>3</sup> )	T (K)	$r_{soap}$ (PGE) (cm <sup>3</sup> /s)	$r_{soap}$ (GMA) (cm <sup>3</sup> /s)	T (K)	$r_{soap}$ (PGE) (cm <sup>3</sup> /s)	$r_{soap}$ (GMA) (cm <sup>3</sup> /s)
DMA	0	333	0.4587	0.4587	353	0.4184	0.4184
	0.1		0.5051	0.5181		0.4975	0.5236
	0.5		0.6623	0.7143		0.7353	0.8130
	1.0		0.8197	0.9009		0.9346	1.0101
	2.0		1.0471	1.1494		1.1765	1.2821
	0	343	0.4717	0.4717	363	0.3610	0.3610
	0.1		0.5405	0.5556		0.4545	0.4902
	0.5		0.7576	0.8130		0.7194	0.8065
	1.0		0.9524	1.0309		0.9174	1.0204
	2.0		1.2048	1.2987		1.1364	1.2346
NMP	0	333	0.3268	0.3268	353	0.4016	0.4016
	0.1		0.3953	0.4082		0.5650	0.5952
	0.5		0.6135	0.6623		1.0000	1.0870
	1.0		0.8065	0.8850		1.3333	1.4493
	2.0		1.0753	1.1905		1.7241	1.9231
	0	343	0.3690	0.3690	363	0.4464	0.4464
	0.1		0.4739	0.4950		0.6897	0.7353
	0.5		0.7813	0.8696		1.2987	1.4085
	1.0		1.0417	1.1628		1.7241	1.8868
	2.0		1.3699	1.5385		2.1739	2.4390
DMSO	0	343	0.2841	0.2841	353	0.4237	0.4237
	0.1		0.3353	0.3425		0.5464	0.5650
	0.5		0.5018	0.5263		0.9025	0.9709
	1.0		0.6540	0.6993		1.1905	1.2903
	2.0		0.8643	0.9346		1.5361	1.6863
	0	353	0.3413	0.3413	363	0.5128	0.5128
	0.1		0.4132	0.4310		0.7210	0.7246
	0.5		0.6390	0.7092		1.2642	1.3158
	1.0		0.8375	0.9259		1.6639	1.7544
	2.0		1.1013	1.2500		2.1008	2.2222

ther purification. Purity of both CO<sub>2</sub> and N<sub>2</sub> was greater than 99.9%. GMA, PGE, imidazole, beomethane, tetraorthosilicate, 3-chloropropyltriethoxysilane, cetyltrimethylammonium bromide, tetramethylammonium chloride, and solvents such as *N,N*-dimethylacetamide (DMA), *N*-methyl-2-pyrrolidinone (NMP), and dimethyl sulfoxide (DMSO) were supplied by Aldrich Chemical Company, U.S.A.

## 2. Absorption Rate of CO<sub>2</sub>

Absorption experiments were carried out in an agitated vessel and the experimental procedure was duplicated in detail as previously reported [24]. The absorption vessel was constructed of glass with an inside diameter of 0.073 m and a height of 0.151 m. Four equally spaced vertical baffles, each one-tenth of the vessel diameter in width, were attached to the internal wall of the vessel. The gas and liquid phase were agitated with an agitator driven by a 1/4 Hp variable speed motor. A straight impeller 0.034 m in length and 0.05 m in width was used as the liquid phase agitator and located at the middle position of the liquid phase. The surface area of the liquid was calculated as the ratio of the volume (300 cm<sup>3</sup>) of added water to the measured height (7.3 cm) of water in the absorber, and was found to be 41.096 cm<sup>2</sup>. The gas and liquid in the vessel were agitated at 50 rpm, which was adequate to maintain a planar gas-

liquid interface. The value of the cumulative volume of the bubbles was measured by a soap bubbler with change in absorption time to obtain the absorption rate of CO<sub>2</sub>. Each experiment was duplicated at least once under identical conditions. The volumetric rising rate ( $r_{soap}$ ) of the bubble in the soap bubbler attached to the absorption vessel was assumed to be equal to the absorption rate of CO<sub>2</sub>. The absorption experiments were carried out in a range of 0–2.0 kmol/m<sup>3</sup> of oxirane and 333–363 K at atmospheric pressure using pure CO<sub>2</sub>, 2 g of catalyst, and solvents such as DMA, NMP and DMSO. The values of  $r_{soap}$  are listed in Table 1.

## 3. Synthesis of ID-CP-MS41

CP-MS41 was synthesized by hydrolysis of tetraorthosilicate, as the silicon source, with 3-chloropropyltriethoxysilane as an organosilane using cetyltrimethylammonium bromide as a template. ID-CP-MS41 was synthesized by immobilization of imidazole on mesoporous CP-MS41. The synthesis of MCM41 and CP-MS41 followed previous work reports [23]. The surface area and size of MCM41 were measured by BET isotherm and SEM, and were measured as 884.6 m<sup>2</sup>/g and 5.0 mm, respectively.

## 4. Physical Properties

The viscosities ( $\mu$ ) of the solvent and oxirane solution were meas-

**Table 2. Physical properties of the CO<sub>2</sub>(A)/PGE and CO<sub>2</sub>(A)/GMA system**

T (K)	Solvent	$C_{Ai}$ (kmol/m <sup>3</sup> )	$\mu$ (cp)	$D_{Ao} \times 10^9$ (m <sup>2</sup> /s)	$D_{PGEo} \times 10^9$ (m <sup>2</sup> /s)	$D_{GMAo} \times 10^9$ (m <sup>2</sup> /s)	$k_{Lo} \times 10^5$ (m/s)
333	DMA	0.0562	0.594	3.921	1.403	3.921	3.990
	NMP	0.0593	0.854	3.283	1.175	1.264	2.697
	DMSO	0.0528	1.082	2.489	0.890	0.959	2.633
343	DMA	0.0494	0.521	4.407	1.577	1.697	4.597
	NMP	0.0587	0.691	3.895	1.393	1.500	3.026
	DMSO	0.0524	0.761	3.242	1.160	1.248	3.136
353	DMA	0.0387	0.468	4.872	1.743	1.876	5.122
	NMP	0.0582	0.603	4.389	1.570	1.690	3.269
	DMSO	0.0520	0.498	4.426	1.583	1.704	3.860
363	DMA	0.0315	0.445	5.181	1.854	1.854	5.344
	NMP	0.0578	0.508	5.060	1.810	1.949	3.601
	DMSO	0.0517	0.345	5.813	2.080	2.080	4.625

ured using a Brookfield viscometer (Brookfield Eng. Lab. Inc, USA).

The solubility ( $C_{Ai}$ ) of CO<sub>2</sub> was measured by the pressure measuring method, which involved measuring the pressure difference of CO<sub>2</sub> before and after equilibrium in the gas and liquid phases, similarly to a previously reported procedure [25], and the experimental procedure was duplicated in detail as previously reported [18].

The diffusivity ( $D_i$ ) of CO<sub>2</sub> and oxiranes in the solvent and solution was estimated by the method modified with viscosity in the Stoke-Einstein equation [26] as follows:

$$D_i = 7.4 \times 10^{-12} \frac{TM_s^{1/2}}{\mu^{2/3} V_i} \quad (17)$$

The experimental data [27] were better correlated through the use of two-thirds power of the viscosity in Eq. (17) rather than a power of 1, as shown in the Stoke-Einstein equation.

The mass transfer coefficients ( $k_{Lo}$ ) of CO<sub>2</sub> in various solvents were obtained from the measured  $r_{sorp}$ . The mass transfer coefficient

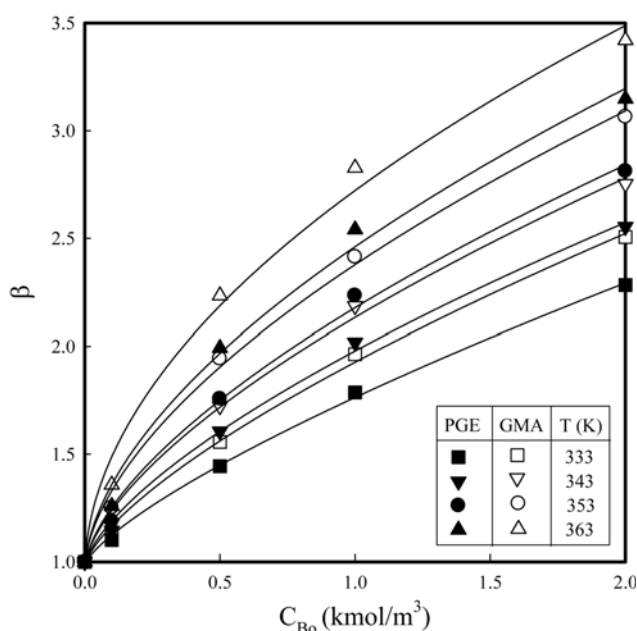
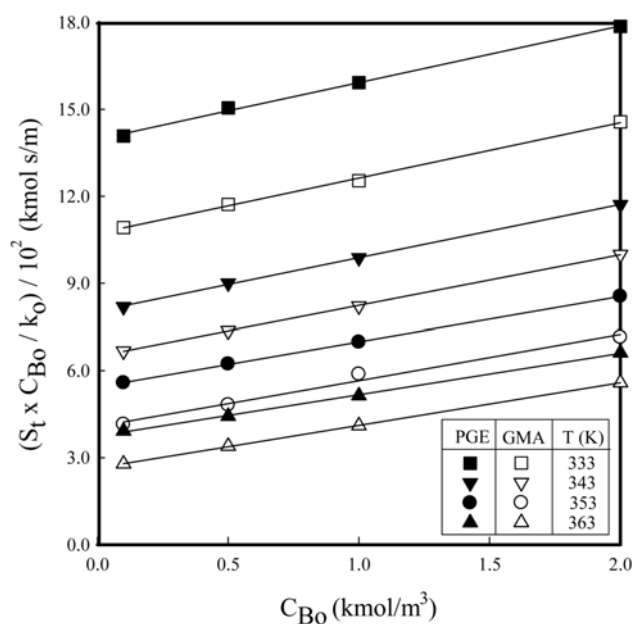
( $k_L$ ) in oxirane solution cannot be measured in the reaction of CO<sub>2</sub> with oxirane. In this study,  $k_L$  was estimated using the relationship [28] between  $k_{Lo}$  and the ratio of diffusivity in solution to that in solvent as follows:

$$k_L = k_{Lo} (D_A/D_{Ao})^{2/3} \quad (18)$$

These physical properties are listed in Table 2, and used to solve the simultaneous differential equations of Eq. (3) and (4).

## RESULTS AND DISCUSSION

The experimental enhancement factor ( $\beta_{exp}$ ) of CO<sub>2</sub> was obtained as the ratio of  $r_{sorp}$  with reaction between CO<sub>2</sub> and oxirane to that without reaction. Fig. 1 shows typical plots of  $\beta_{exp}$  against  $C_{Bo}$  in DMA solution at various absorption temperatures for PGE and GMA, and demonstrates that  $\beta_{exp}$  increases with increasing  $C_{Bo}$  and temperature. These results are similar for other solvents. The solid line

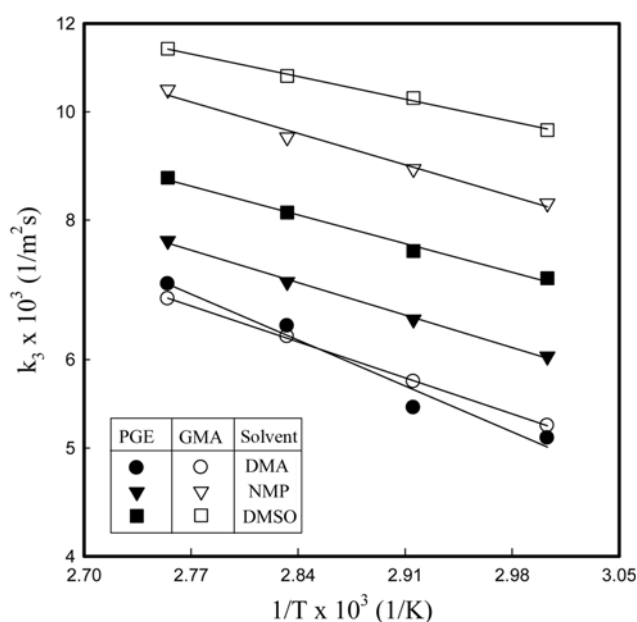
**Fig. 1.  $\beta$  vs.  $C_{Bo}$  in DMA solution for PGA and GMA.****Fig. 2.  $S_t C_{Bo} / k_o$  vs.  $C_{Bo}$  in DMA solution for PGE and GMA.**

presents the calculated value ( $\beta_{cal}$ ) of  $\beta$ , to be discussed later.  $\beta_{exp}$  of GMA were a little larger than those of PGE.

The measured  $\beta_{exp}$  and Eq. (15) give  $k_o$ , and then,  $K_1$  and  $k_3$  are evaluated from the slope and intercept of the plots of  $C_{Bo}S_i/k_o$  against

**Table 3. Reaction rate constants of the reaction between CO<sub>2</sub> and oxirane**

Oxirane	Temp. (K)	Solvent	$k_3 \times 10^3$ (1/m <sup>2</sup> ·s)	$K_1$ (m <sup>3</sup> /kmol)
PGE	333	DMA	5.104	0.140
		NMP	6.041	0.137
		DMSO	7.097	0.126
	343	DMA	5.433	0.229
		NMP	6.518	0.187
		DMSO	7.506	0.153
	353	DMA	6.430	0.286
		NMP	7.043	0.264
		DMSO	8.127	0.221
GMA	363	DMA	7.011	0.381
		NMP	7.668	0.356
		DMSO	8.730	0.325
	333	DMA	5.236	0.178
		NMP	8.281	0.120
		DMSO	9.632	0.105
	343	DMA	5.735	0.268
		NMP	8.890	0.169
		DMSO	10.29	0.140
	353	DMA	6.292	0.390
		NMP	9.492	0.231
		DMSO	10.77	0.193
	363	DMA	6.801	0.556
		NMP	10.47	0.307
		DMSO	11.39	0.259



**Fig. 3. Arrhenius plot of  $k_3$  for PGE and GMA.**

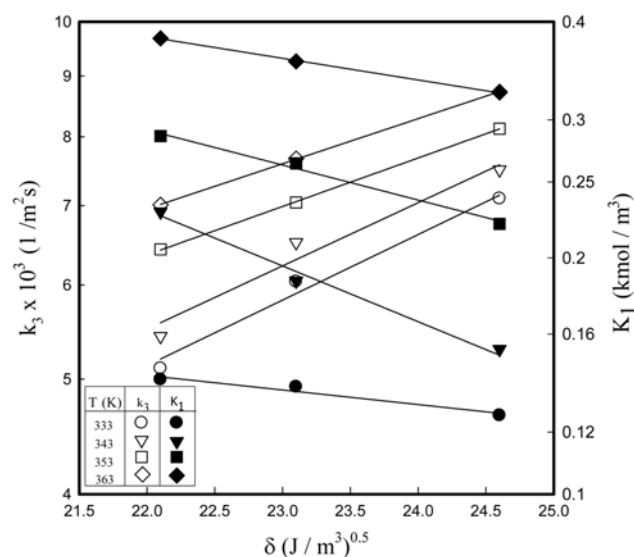
$C_{Bo}$  according to Eq. (16). Typical plots of  $S_i C_{Bo}/k_o$  against  $C_{Bo}$  are presented in Fig. 2 for the same conditions as shown in Fig. 1. The linear plots allow  $k_3$  and  $K_1$  to be obtained from the slope and intercept of the straight line according to Eq. (16), respectively. These results are similar for other solvents. The values of  $k_3$  and  $K_1$  for various solvents and temperatures are listed in Table 3. From the results of little difference of  $\beta_{exp}$  in Fig. 1, and  $k_3$  and  $K_1$  in Table 3, it seems that the intermediate complex of PGE and that of GMA in reaction (ii) have similar characteristics of electron formation to react with CO<sub>2</sub>.

Fig. 3 shows the Arrhenius plots of  $k_3$  with parameters of solvents and oxirane. The Arrhenius plots are linear and linear regression analysis of the Arrhenius plots with  $r^2 > 0.960$  gives the activation energy for the forward reaction rate constant in the irreversible reaction of (iii), with 11.2, 8.0, and 7.0 kJ/mol for PGE and 8.8, 7.7, 5.5 kJ/mol for GMA in solvents of DMA, NMP, and DMSO, respectively.

Various empirical measurements of solvent effects have been proposed and correlated with the reaction rate constant [29]. Some measurements have a linear relationship to the solubility parameter ( $\delta$ ) of the solvent with logarithms of  $k_3$  and  $K_1$  plotted against  $\delta$  [30] of DMA, NMP, and DMSO (18.2, 23.1, 24.6 (J/m<sup>3</sup>)<sup>0.5</sup>), respectively, in Fig. 4 and Fig. 5 for PGE and GMA, respectively.

The plots are linear, and  $k_3$  and  $K_1$  increase and decrease with higher  $\delta$  respectively. The solvent polarity increased with higher  $\delta$ . Presumably, the increased instability and solvation of complex ( $C_1$ ), arising from increased solvent polarity, enhance the dissociation reaction of  $C_1$  and the reaction between  $C_1$  and CO<sub>2</sub>, as in an SN<sub>1</sub> (nucleophilic substitution) reaction [31]. The results in these figures suggest that the magnitude of the rate constants may be a function of the stabilization of the zwitterionic intermediates by the solvent [4]. The linear dependence of rate constant on  $\delta$  as shown in these figures, could be used to predict the rate constant in any organic solvent with  $\delta$ .

Using the obtained values of  $k_3$  and  $K_1$  at given  $C_{Bo}$ ,  $C_{Ais}$ ,  $D_A$ ,  $D_B$ , and  $k_L$ , The simultaneous differential equations of Eq. (8) and (9)



**Fig. 4. Relationship between reaction rate constant and various solvent solubilities for PGE.**

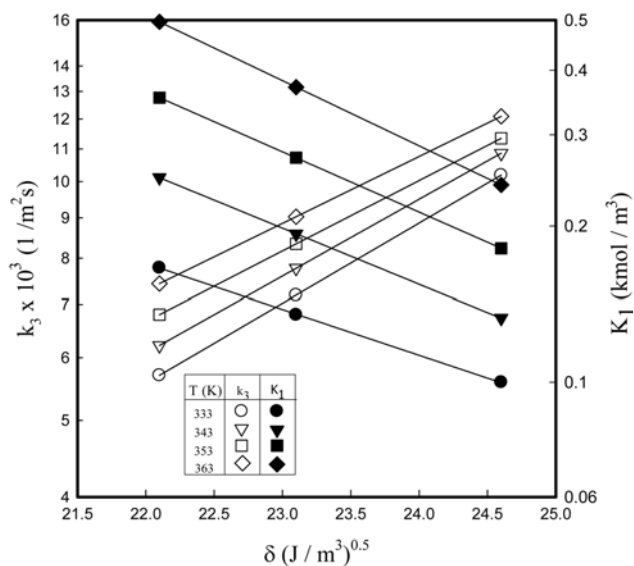


Fig. 5. Relationship between reaction rate constant and various solvent solubilities for GMA.

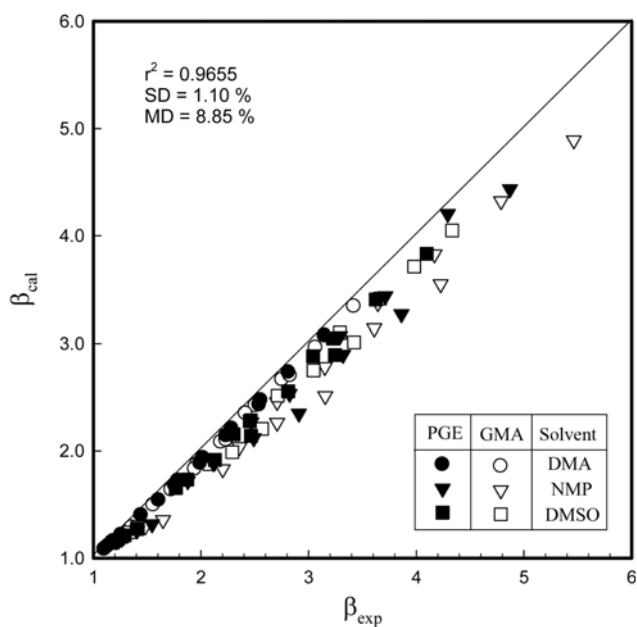


Fig. 6. Comparison of the calculated and measured values of the enhancement factor of CO<sub>2</sub> for PGE and GMA.

with boundary conditions of Eq. (10) and (11) were numerically solved by a finite element method to give the profiles of  $C_A$  and  $C_B$ , and then, the  $\beta_{cal}$  was calculated from Eq. (12). Typical values are shown as symbols of the solid line in Fig. 1 and  $\beta_{exp}$  approaches to  $\beta_{cal}$ . All values of  $\beta_{exp}$  and  $\beta_{cal}$  for various solvents, oxirane concentrations and temperatures were compared in Fig. 6.  $\beta_{exp}$  approached  $\beta_{cal}$  within a mean deviation of 1.23% with  $r^2$  of 0.96.

To observe the effect of physicochemical properties on  $\beta$ ,  $\beta$  was obtained for various dimensionless variable of physicochemical properties such as  $q$ ,  $M$ ,  $\alpha$  and  $a_L$  through the solution of the simultaneous differential equations of Eq. (8) and (9).

$\beta$ , calculated from Eq. (12), were plotted for various  $q$  under the

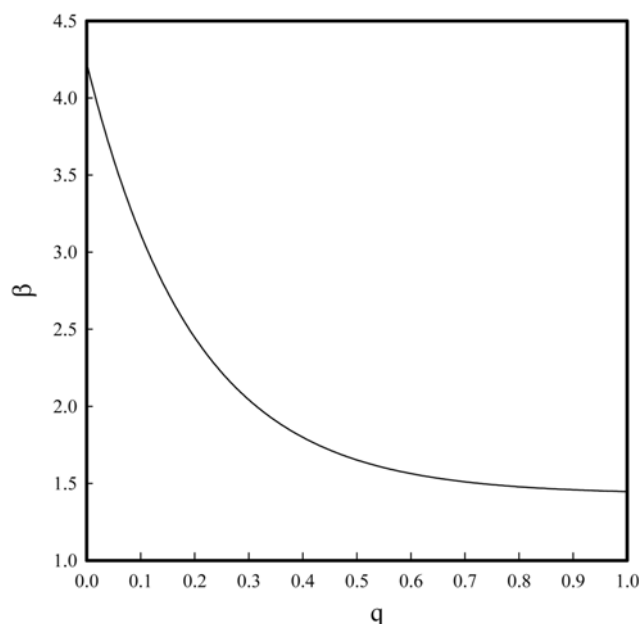


Fig. 7. Effect of  $q$  on  $\beta$  for  $M=20$ ,  $a=0.1$ ,  $a_L=0.0001$ , and  $r_{AB}=2.6$ .

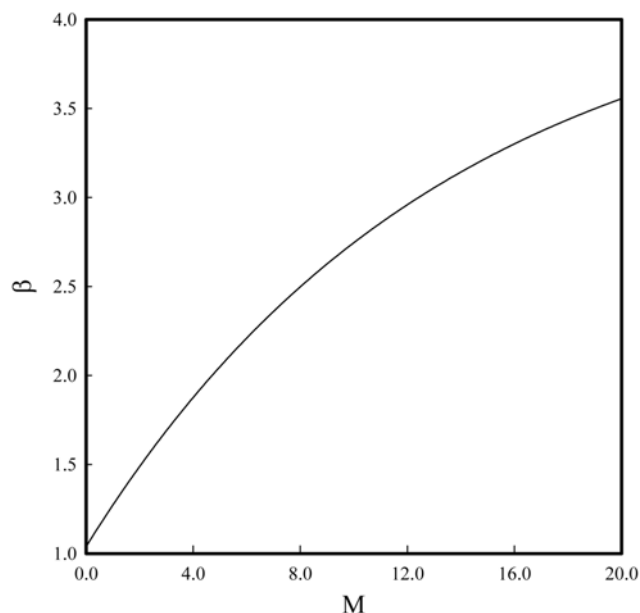


Fig. 8. Effect of  $M$  on  $\beta$  for  $q=0.05$ ,  $a_L=0.0001$ ,  $\alpha=0.1$ , and  $r_{AB}=2.6$ .

typical conditions of  $M$  of 20,  $\alpha$  of 0.1,  $a_L$  of 0.0001, and  $r_{AB}$  of 2.6 in Fig. 7.  $\beta$  decreased with increasing  $q$ . This means that  $\beta$  decrease with increasing the physical absorption rate due to increase of  $C_{Ai}$  or decreasing the chemical absorption rate due to decrease of  $C_{Bo}$  by increase of  $q$ .

$\beta$ , calculated from Eq. (12), were plotted for various  $M$  under the typical conditions of  $q$  of 0.05,  $\alpha$  of 0.1,  $a_L$  of 0.0001, and  $r_{AB}$  of 2.6 in Fig. 8.  $\beta$  increased with increasing  $M$ , which means that  $\beta$  increase with increasing the chemical absorption rate due to increase of  $k_3$ ,  $C_{Bo}$  and  $S_b$ , or decreasing the physical absorption rate due to decrease of  $k_L$  by increase of  $M$ .

$\beta$ , calculated from Eq. (12), were plotted for various  $a$  under the

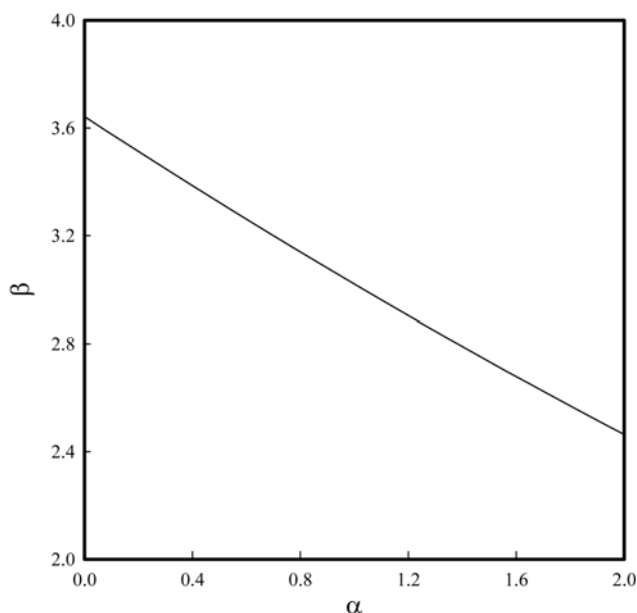


Fig. 9. Effect of  $\alpha$  on  $\beta$  for  $M=20$ ,  $q=0.05$ ,  $a_L=0.0001$ , and  $r_{AB}=2.6$ .

typical conditions of  $q$  of 0.05,  $M$  of 20,  $a_L$  of 0.0001, and  $r_{AB}$  of 2.6 in Fig. 9.  $\beta$  decreased with increasing  $\alpha$ .  $\beta$  should increase by increase of  $K_1$  or  $C_{B_0}$  due to increase of  $\alpha$ , as shown in Eq. (ii). From the definition of  $M$ , the other quantities,  $k_3 D_A S_i / k_L^2$ , except  $\alpha$  in  $M$  decrease with increasing  $\alpha$  at the given value of  $M$ . Therefore, increase of the chemical absorption rate due to decrease of  $k_3$ ,  $C_{B_0}$  and  $S_i$ , or increase of the physical absorption rate due to increase of  $k_L$  make  $\beta$  decreased as shown in Fig. 9.

$\beta$ , calculated from Eq. (12), were plotted for various  $\alpha$  under the typical conditions of  $q$  of 0.05,  $M$  of 20,  $a_L$  of 0.0001, and  $r_{AB}$  of 2.6 in Fig. 10.  $\beta$  was almost constant with increasing  $a_L$  from which it could be concluded that the effect of  $a_L$  on  $\beta$  is little.

$\beta$ , calculated from Eq. (12), were plotted for various  $r_{AB}$  under the

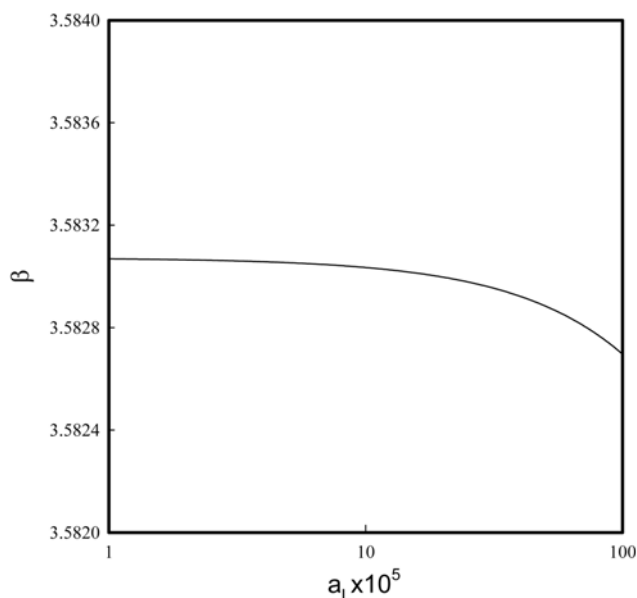


Fig. 10. Effect of  $a_L$  on  $\beta$  for  $M=20$ ,  $q=0.05$ ,  $\alpha=0.1$ , and  $r_{AB}=2.6$ .

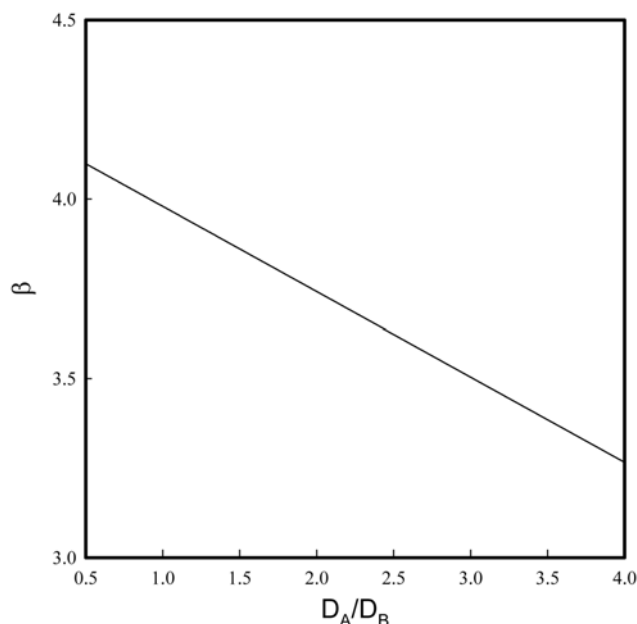


Fig. 11. Effect of  $r_{AB}$  on  $\beta$  for  $M=20$ ,  $q=0.05$ ,  $\alpha=0.1$ , and  $a_L=0.0001$ .

typical conditions of  $q$  of 0.05,  $M$  of 20,  $\alpha$  of 0.1, and  $a_L$  of 0.0001 in Fig. 11.  $\beta$  decreased with increasing  $r_{AB}$ . This means that  $\beta$  decrease due to decrease of mobility of oxirane by increase of the ratio of  $D_A$  to  $D_B$ .

## CONCLUSIONS

Carbon dioxide was absorbed to react with oxiranes in solvent of DMA, NMP, and DMSO. A mathematical model for the  $\text{CO}_2$  absorption associated with reaction with the oxirane was developed on the basis of the film theory with a non-linear reaction rate equation according to the zwitterion mechanism. Absorption data of  $\text{CO}_2$  were used to obtain pseudo-first-order reaction rate constants, from which the elementary reaction rate constants were evaluated. The logarithmic reaction constants showed close to linear dependence on the solubility parameter of the solvent. The solution of dimensionless simultaneous differential equation for  $\text{CO}_2$  and oxirane could predict the enhancement factor of  $\text{CO}_2$  using the experimental variables. The reactivity of PGE with  $\text{CO}_2$  is similar to that of GMA from the comparison of  $k_3$  and  $K_1$ .

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## NOMENCLATURE

- $a_v$  : ratio of interfacial area of liquid to liquid volume [1/m]
- $C_i$  : concentration of species  $i$  [kmol/m<sup>3</sup>]
- $D_i$  : diffusivity of species  $i$  [m<sup>2</sup>/s]
- $H_a$  : Hatta number defined as  $\sqrt{k_3 D_A / k_L}$

$k_o$	: pseudo-first-order reaction rate constant [1/s]
$K_1$	: reaction equilibrium constant defined as $k_1/k_2$ [ $\text{m}^3/\text{kmol}$ ]
$k_1$	: forward reaction rate constant in reaction (ii) [ $1/\text{m}^2\cdot\text{s}$ ]
$k_2$	: backward reaction rate constant in reaction (ii) [ $\text{kmol}/\text{m}^3\cdot\text{m}^2\cdot\text{s}$ ]
$k_3$	: forward reaction rate constant in reaction (iii) [ $1/\text{m}^2\cdot\text{s}$ ]
$k_L$	: liquid-side mass transfer coefficient of $\text{CO}_2$ with reaction [m/s]
$k_{Lo}$	: liquid-side mass transfer coefficient of $\text{CO}_2$ in solvent [m/s]
$M_S$	: molecular weight of solvent [g/gmole]
$r^2$	: correlation coefficient
$r_A$	: reaction rate of $\text{CO}_2$ [ $\text{kmol}/\text{m}^3\cdot\text{s}$ ]
$r_{\text{soup}}$	: volumetric rising rate of the soup bubble [ $\text{cm}^3/\text{s}$ ]
$S_t$	: surface area of catalyst [ $\text{m}^2$ ]
$t$	: absorption time [s]
$T$	: absorption temperature [K]
$z$	: distance [m]
$z_L$	: film thickness [m]

### Greek Letters

$\beta$	: enhancement factor of $\text{CO}_2$
$\delta$	: solubility parameter of solvent ( $\text{J}/\text{m}^3$ ) <sup>1/2</sup>
$\mu$	: viscosity of liquid [cP]

### Subscripts

A	: $\text{CO}_2$
B	: PGE or GMA
cal	: calculated value
exp	: measured value
i	: gas-liquid interface or species i
o	: feed or solvent

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