

## Mechanism of Ce promoting SO<sub>2</sub> resistance of MnO<sub>x</sub>/γ-Al<sub>2</sub>O<sub>3</sub>: An experimental and DFT study

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**Abstract**—Various physico-chemical techniques and theoretical chemistry computations are used to obtain a deep insight into the mechanism of Ce improving SO<sub>2</sub> resistance of the catalyst Mn<sub>0.4</sub>Ce<sub>x</sub>/Al<sub>2</sub>O<sub>3</sub> (x stands for the molar ratio of Ce : Al). Theoretical computation with density functional theory (DFT) shows that Ce modification enhances the adsorption energy of SO<sub>2</sub> adsorbed on Ce surrounding, resulting in the preferential adsorption of SO<sub>2</sub> on Ce surrounding. It protects the surface Mn from SO<sub>2</sub> poisoning, leading to a better SO<sub>2</sub> resistance. FT-IR and TG results are in good accordance with DFT results. FT-IR results suggest that absorption peaks related to SO<sub>4</sub><sup>2-</sup> cannot be detected in Mn<sub>0.4</sub>Ce<sub>0.12</sub>/Al<sub>2</sub>O<sub>3</sub>. Moreover, TG results show that weight loss peaks due to sulfated MnO<sub>x</sub> decomposition disappears after Ce addition. Therefore, Ce modification inhibits sulfates formation on active components lead to a better resistance to SO<sub>2</sub> of Mn<sub>0.4</sub>Ce<sub>0.12</sub>/Al<sub>2</sub>O<sub>3</sub>.

Keywords: Selective Catalytic Reduction, MnO<sub>x</sub>, Density Functional Theory, Modification, SO<sub>2</sub> Poisoning

### INTRODUCTION

Selective catalytic reduction (SCR) with NH<sub>3</sub> in the presence of oxygen is a feasible technique to reduce NO<sub>x</sub> emissions in stationary power plants [1]. V<sub>2</sub>O<sub>5</sub>-WO<sub>3</sub>/TiO<sub>2</sub> catalysts are most commonly adopted [2,3]. To avoid reheat flue gas, the SCR unit has to be located upstream of the desulfurizer and the electrostatic precipitator resulting in a deactivation of catalysts due to dust and alkali metals in flue gas. Low-temperature SCR catalysts can be located downstream and help to prevent the SCR unit from suffering these problems.

MnO<sub>x</sub> based catalysts supported on various supports such as TiO<sub>2</sub> [1,2], TiO<sub>2</sub>-pillared clay [4], γ-Al<sub>2</sub>O<sub>3</sub> [5-7], (active carbon) AC [8], Ce-ZrO<sub>2</sub> [9,10] and some other non-supported catalysts, Mn-Ce [11,12], MnO<sub>2</sub>-Fe<sub>2</sub>O<sub>3</sub>-CeO<sub>2</sub>-TiO<sub>2</sub> [13] have been reported in recent years, and these MnO<sub>x</sub> based catalysts were found to have an excellent SCR activity at low temperature. Unfortunately, there are still a few amounts of SO<sub>2</sub> even after the desulfurizer. MnO<sub>x</sub> based catalysts are sensitive to SO<sub>2</sub> and can be deactivated by formation of sulfite and sulfate species on the catalyst surface [14].

Modifying with cerium can improve SO<sub>2</sub> resistance for MnO<sub>x</sub> based catalysts to a certain extent. Cao et al. [15] prepared Fe-Mn-Ce/γ-Al<sub>2</sub>O<sub>3</sub> using the sol-gel method and found that the catalyst had a favorable SO<sub>2</sub> and H<sub>2</sub>O resistance and the SCR activity remained above 75% in the presence of SO<sub>2</sub> and H<sub>2</sub>O. Some other MnO<sub>x</sub> based catalysts doped with cerium such as Mn-Ce/γ-Al<sub>2</sub>O<sub>3</sub>

[7], MnO<sub>x</sub>/CeO<sub>2</sub>-TiO<sub>2</sub> [2], MnO<sub>2</sub>-Fe<sub>2</sub>O<sub>3</sub>-CeO<sub>2</sub>-TiO<sub>2</sub> [13], Mn/Ce-ZrO<sub>2</sub> [16] also show a better SO<sub>2</sub> resistance. The mechanism of cerium improving SO<sub>2</sub> resistance has been researched. Chang et al. [11] investigated the resistance to SO<sub>2</sub> of MnO<sub>x</sub>-CeO<sub>2</sub> and pointed out that the high concentration of surface oxygen vacancy corresponded to a better SO<sub>2</sub> resistance. Zhang et al. [17] prepared CeO<sub>2</sub> catalysts modified with solid acid and found that the resistance to H<sub>2</sub>O and SO<sub>2</sub> of the catalysts depended on the improvement of surface acidity. Wu et al. [18] and Jin et al. [19] pointed out that cerium addition improved the dissociation of ammonium sulfate on the catalyst surface, resulting in a better SO<sub>2</sub> resistance. SO<sub>2</sub> poisoning starts with the adsorption of SO<sub>2</sub> on the catalyst surface, and then reacts with NH<sub>3</sub> or catalyst components to form some sulfite or sulfate species. This process is closely related to the surface structure of catalysts. Ce doping changes the surface structural properties of catalysts [2,20], which may affect the SO<sub>2</sub> adsorption and the stability of sulfite or sulfate species on the catalyst surface and then affect the SO<sub>2</sub> resistance. However, very little information about this part was available in previous studies.

Therefore, in this work, MnO<sub>x</sub>/γ-Al<sub>2</sub>O<sub>3</sub> catalyst doped with CeO<sub>2</sub> was prepared and used to remove NO at low temperature in the presence of SO<sub>2</sub>. DFT calculation and physicochemical characterizations were performed to get a deep insight into the Ce doping effect on SO<sub>2</sub> adsorption and the stability of sulfite or sulfate species on catalysts surface and to reveal the mechanism of Ce improving SO<sub>2</sub> resistance of the catalyst.

### 1. Experimental

#### 1-1. Preparation of Supports and Catalysts

Catalyst support was prepared by precipitation method. Al(NO<sub>3</sub>)<sub>3</sub>·

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9H<sub>2</sub>O as a precursor was dissolved in distilled water. An aqueous solution of ammonia with 25 wt% as the precipitator was added dropwise into the solution until the pH was up to 10. The resulting precipitate was stirred for 3 h and then aged for 1 h and finally filtered, washed, and dried in water bath at 80 °C overnight to get support powder.

Catalysts were prepared by impregnating support powder with Mn(NO<sub>3</sub>)<sub>2</sub> solution or mixed solutions of Mn(NO<sub>3</sub>)<sub>2</sub> and Ce(NO<sub>3</sub>)<sub>3</sub>·6H<sub>2</sub>O for 12 h. Then the samples were dried in water bath at 80 °C overnight and dried in drying oven at 110 °C for 6 h and finally were calcined in muffle at 500 °C for 6 h. The catalysts were denoted as Mn<sub>x</sub>Ce<sub>y</sub>/Al<sub>2</sub>O<sub>3</sub>, where x and y stand for the molar ratios of Mn : Al and Ce : Al.

All chemicals were obtained from Tianjin Guangfu Fine Chemical Research Institute (China).

### 1-2. Characterization of Supports and Catalysts

BET surface areas of the catalysts were measured by nitrogen adsorption at -196 °C using a Autosorb-iQ-C automated gas sorption system (Quantachrome Instruments, USA). The pore size distribution was calculated from the desorption branch of the N<sub>2</sub> adsorption isotherm using the Barrett-Joyner-Halenda (BJH) formula. Prior to the measurements, all samples were outgassed at 300 °C for 2 h.

The powder X-ray diffraction (XRD) measurement was used to identify the crystal structure of the catalysts with XRD-7000 S system using Cu K $\alpha$  radiation (40 kV, 100 mA) (SHIMADZU Corporation, Japan). Diffraction patterns were obtained over a 2 $\theta$  range of 8-80°, at a scan speed of 5° min<sup>-1</sup> and a step of 0.02°.

The change of the relative atomic concentration on the surface of the catalysts were obtained by the X-ray photoelectron spectroscopy using a ESCALAB250 (Thermo Fisher Scientific Corporation, USA) with monochromatic AlK $\alpha$  radiation. Sample charging effects were eliminated by correcting the observed spectra with the C 1s binding energy value of 284.6 eV.

FT-IR spectra were acquired with a Nicolet iN10 MX & iS10 (ThermoFisher) FT-IR spectrometer using a thin self-supporting sample wafer accumulation of 100 scans running at 4 cm<sup>-1</sup> resolution.

Thermogravimetric analyses (TGA) were performed on 0.01 g of sample with a NETZSCH thermal analysis system under a nitrogen flow of 20 mL/min, using a heating rate of 10 °C/min from room temperature to 900 °C (NETZSCH Corporation, Germany).

### 1-3. Catalytic Activity Test

The SCR activity measurement was performed in a fixed-bed flow reactor (Fig. S1). The concentrations of simulated gases were as follow: 600 ppm NO, 600 ppm NH<sub>3</sub>, 3 vol% O<sub>2</sub>, 3 vol% H<sub>2</sub>O (when used), 100 ppm SO<sub>2</sub> (when used) and N<sub>2</sub> as balance gas. In all the runs, the total gas flow rate was 300 mL/min and the gas hourly space velocity (GHSV) was about 45,000 h<sup>-1</sup>. The feed gases were mixed and preheated in a chamber before entering the reactor. The water vapor was generated by passing N<sub>2</sub> through a gas-wash bottle containing deionized water. During the measurements, the concentrations of NO at the inlet and outlet of the reactor were monitored by flue gas analyzer (KM950, Kane International Ltd., United Kingdom). The concentration of N<sub>2</sub>O was measured by FTIR (WQF-510A, Beijing Rayleigh Analytical Instrument Co.,

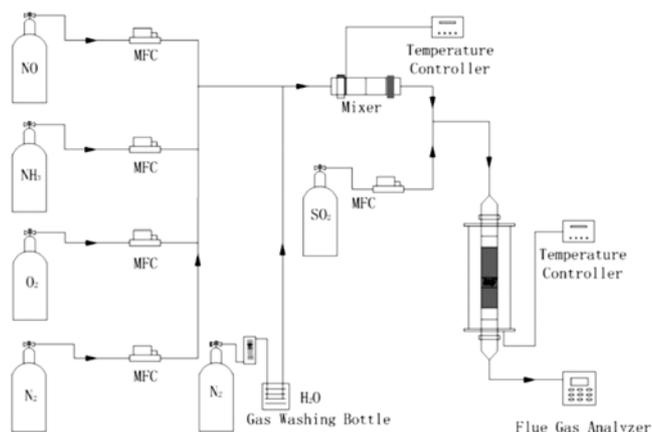


Fig. 1. Schematic diagram of the experimental setup.

Ltd.) equipped with a gas sample cell. The NO conversion was calculated using the following equation:

$$\text{NO conversion \%} = \frac{\text{NO}_{in} - \text{NO}_{out}}{\text{NO}_{in}} \times 100\%$$

NO<sub>in</sub>: inlet NO<sub>x</sub> concentration (ppm); NO<sub>out</sub>: outlet NO<sub>x</sub> concentration (ppm)

### 1-4. Models and Computational Details

All calculations were carried out with the Material Studio modelling Dmol3 package [21,22]. Double numerical plus polarization function (the DNP basis set) and the generalized gradient approximation (GGA) with PBE functional were used in all calculations [22,23]. And the real space cut-off radius was maintained as 5.8 Å. The core electrons were treated with DFT semi-core pseudopotentials. Models were built with six atomic layers with two bottom layers fixed and four top layers relaxed. The vacuum region was set to be 18 Å. The lattice constant of MnO<sub>2</sub> is a=b=4.3983, c=2.8730 Å and  $\alpha=\beta=\gamma=90^\circ$  [24]. And that of CeO<sub>2</sub> is a=b=c=5.411 Å and  $\alpha=\beta=\gamma=90^\circ$  [25]. The tolerance of energy is 0.00027 eV, gradient is 0.054 eV/Å, smearing is 0.136 eV, and displacement convergence is 0.005 Å.

The adsorption energy ( $E_{ads}$ ) was calculated as follows:  $E_{ads} = E_{SO_2/Surface} - (E_{SO_2} + E_{Surface})$ , where  $E_{Surface}$  is the total energy of bare MnO<sub>2</sub> (110) or CeO<sub>2</sub> (110),  $E_{SO_2}$  is the energy of an isolated SO<sub>2</sub> molecule and  $E_{SO_2/Surface}$  is the total energy of the same molecule adsorbed on surface.

## RESULTS AND DISCUSSION

### 1. Catalytic Activity Results

NO conversions of the catalysts in temperature range from 80 to 240 °C are shown in Fig. 2(a). The activity for Mn<sub>0.4</sub>/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> increased with the increase of temperature, reached a maximum value 99.5% at 180 °C and then decreased. After the addition of Ce, the SCR activity was dramatically improved, especially at low temperature. NO removal efficiency of Mn<sub>0.4</sub>Ce<sub>0.12</sub>/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> was 70.8% at 80 °C, which was 41.7% more than that of Mn<sub>0.4</sub>/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> at the same temperature. And it maintained at 100% in the temperature range of 100-240 °C.

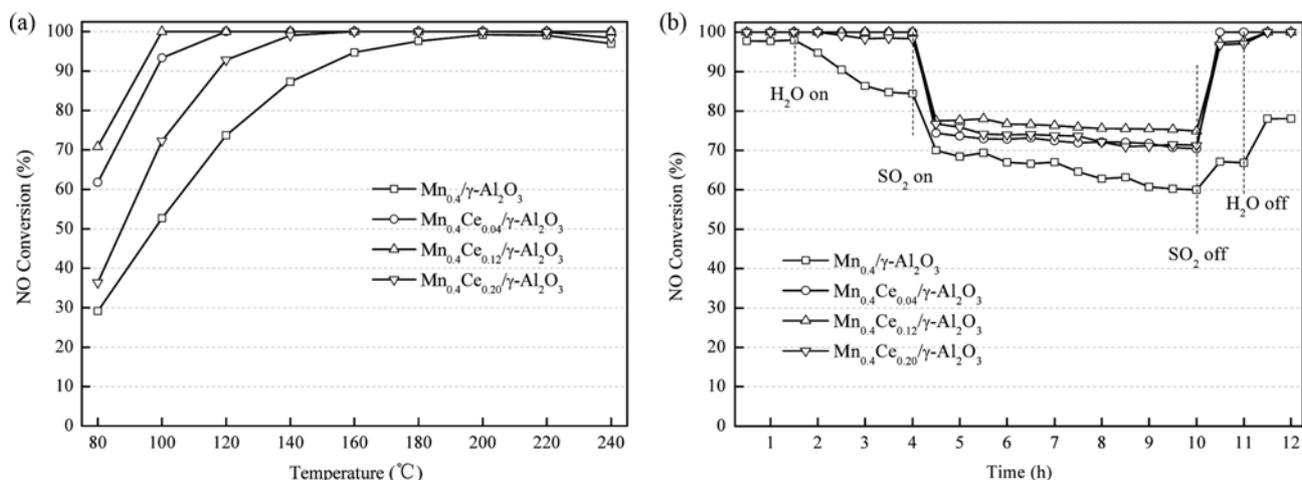


Fig. 2. (a) SCR activity of different catalysts (b) Effect of H<sub>2</sub>O and SO<sub>2</sub> on SCR activity of different catalysts at 180 °C of different catalysts.

There was still a small amount of SO<sub>2</sub> and H<sub>2</sub>O in flue gases after desulfurization, which may inhibit SCR activity to some degree. Therefore, an experiment was designed to investigate the effect of SO<sub>2</sub> and H<sub>2</sub>O on the SCR activity, and the results are illustrated in Fig. 2(b). For Mn<sub>0.4</sub>/γ-Al<sub>2</sub>O<sub>3</sub>, the activity decreased slowly from 98.0% to 84.4% in 2.5 h after the addition of H<sub>2</sub>O. When SO<sub>2</sub> was added into the flue gas, the activity sharply decreased from 84.4% to 70.0% in the first 0.5 h and then the activity declined slowly to 60% during 5.5 h. When SO<sub>2</sub> and H<sub>2</sub>O were cut off, the activity partly recovered. After Ce doping, the NO removal efficiency for these catalysts remained at about 100% in the presence of H<sub>2</sub>O at 180 °C. When SO<sub>2</sub> was injected, the activity decreased to 70.0% in the first 0.5 h and then kept stable. When SO<sub>2</sub> and H<sub>2</sub>O were cut off, the activity totally recovered to the original level. Compared to Mn<sub>0.4</sub>Ce<sub>0.04</sub>/γ-Al<sub>2</sub>O<sub>3</sub> and Mn<sub>0.4</sub>Ce<sub>0.2</sub>/γ-Al<sub>2</sub>O<sub>3</sub>, Mn<sub>0.4</sub>Ce<sub>0.12</sub>/γ-Al<sub>2</sub>O<sub>3</sub> had a little higher NO removal efficiency in the presence of SO<sub>2</sub> and H<sub>2</sub>O. These results suggested that Ce doping, especially when the ratio Ce:Al was 0.12:1, significantly improved the resistance to H<sub>2</sub>O and SO<sub>2</sub> of the catalyst.

## 2. Catalyst Characterization and DFT Calculation

### 2-1. BET and XRD Analysis

The BET surface area, pore volume, and pore size of different samples are summarized in Table 1. The BET surface area, pore volume, and pore size of Mn<sub>0.4</sub>/γ-Al<sub>2</sub>O<sub>3</sub> was 175.4 m<sup>2</sup>/g, 0.269 cm<sup>3</sup>/g and 6.13 nm, respectively. Ce addition could enhance BET surface area and pore size and the maximum values turned up in Mn<sub>0.4</sub>Ce<sub>0.12</sub>/γ-Al<sub>2</sub>O<sub>3</sub> which were 231.8 m<sup>2</sup>/g and 0.380 cm<sup>3</sup>/g, respectively. It indicated that, to certain extent, Ce addition could improve

Table 1. Specific surface area and pore structure of the catalyst

Sample	BET surface area (m <sup>2</sup> /g)	Pore volume (cm <sup>3</sup> /g)	Pore size (nm)
Mn <sub>0.4</sub> /γ-Al <sub>2</sub> O <sub>3</sub>	175.4	0.269	6.13
Mn <sub>0.4</sub> Ce <sub>0.04</sub> /γ-Al <sub>2</sub> O <sub>3</sub>	200.0	0.364	7.28
Mn <sub>0.4</sub> Ce <sub>0.12</sub> /γ-Al <sub>2</sub> O <sub>3</sub>	231.8	0.380	6.56
Mn <sub>0.4</sub> Ce <sub>0.20</sub> /γ-Al <sub>2</sub> O <sub>3</sub>	175.1	0.289	6.59

the dispersion of MnO<sub>2</sub>. However, when Ce loading amount further increased, BET surface area and pore size decreased. Pure ceria has been known to be poorly thermostable and easily sintering under high temperature [26,27]. Excessive Ce loading might weaken the interaction between Ce and Mn, resulting in Ce sintering and a small BET surface area and pore size.

XRD patterns of the catalysts are shown in Fig. 3. Four sharp and strong peaks at  $2\theta=28.7, 37.1, 42.4, 56.6, 66.0, 72.3$  were detected in the catalyst Mn<sub>0.4</sub>/γ-Al<sub>2</sub>O<sub>3</sub> and were attributed to the phase of MnO<sub>2</sub> (JCPDS no. 30-0820 and 24-0735). After Ce addition, those peaks became much weaker due to the interaction between Ce and Mn [18,28]. When Ce loading amount reached 0.2, MnO<sub>2</sub> diffraction peaks became strong. These results suggest that the optimal Ce loading amount for Mn<sub>0.4</sub>/γ-Al<sub>2</sub>O<sub>3</sub> was 0.12. The grain size of MnO<sub>2</sub> in Mn<sub>0.4</sub>/γ-Al<sub>2</sub>O<sub>3</sub>, Mn<sub>0.4</sub>Ce<sub>0.04</sub>/γ-Al<sub>2</sub>O<sub>3</sub>, Mn<sub>0.4</sub>Ce<sub>0.12</sub>/γ-Al<sub>2</sub>O<sub>3</sub> and Mn<sub>0.4</sub>Ce<sub>0.2</sub>/γ-Al<sub>2</sub>O<sub>3</sub> was 92.4, 79.8, 67.4 and 84.0 Å, respectively, which were calculated by the Scherrer Formula and K value was 0.943. Note that values of grain size obtained from the Scher-

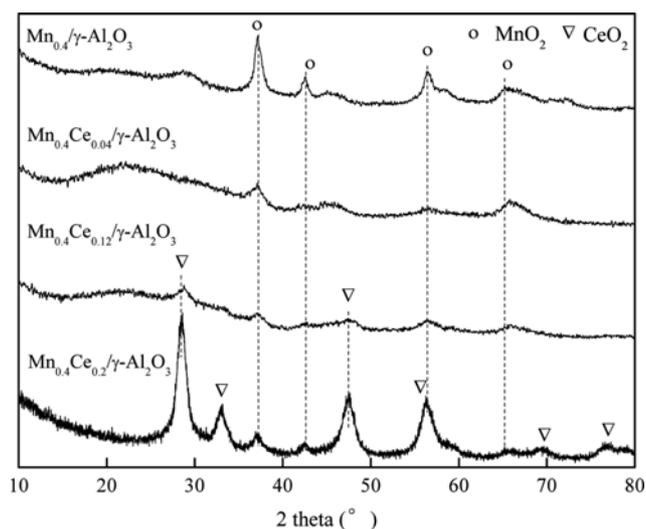


Fig. 3. XRD patterns of different catalysts.

rer formula were not accurate, but from these results we could still tell the better dispersion of  $\text{MnO}_2$  in  $\text{Mn}_{0.4}\text{Ce}_{0.12}/\gamma\text{-Al}_2\text{O}_3$  because of Ce adding. Compared to  $\text{Mn}_{0.4}/\gamma\text{-Al}_2\text{O}_3$ , new peaks at  $2\theta=28.5, 33.1, 47.5, 56.3, 69.4$  and  $76.7$  were detected in the catalyst  $\text{Mn}_{0.4}\text{Ce}_{0.2}/\gamma\text{-Al}_2\text{O}_3$  and were attributed to the phase of  $\text{CeO}_2$  (JCPDS no. 43-1002). But for  $\text{Mn}_{0.4}\text{Ce}_{0.04}/\gamma\text{-Al}_2\text{O}_3$  and  $\text{Mn}_{0.4}\text{Ce}_{0.12}/\gamma\text{-Al}_2\text{O}_3$ ,  $\text{CeO}_2$  diffraction peaks were not apparent and even could not be detected. Those results indicated that Ce modification could improve the dispersion of  $\text{MnO}_2$ , but when the Ce loading amount increased, both  $\text{CeO}_2$  and  $\text{MnO}_2$  dispersion got worse. The high dispersion and poor crystal structure  $\text{CeO}_2$  and  $\text{MnO}_2$  in  $\text{Mn}_{0.4}\text{Ce}_{0.12}/\gamma\text{-Al}_2\text{O}_3$  were favorable for the SCR activity as reported in previous works [29,30].

## 2-2. XPS Analysis

XPS analyses were performed to identify the surface properties of the catalysts. The XPS spectra of Mn 2p, Ce 3d and O 1s are shown in Fig. 4 and the surface atomic concentrations are shown in Table 2.

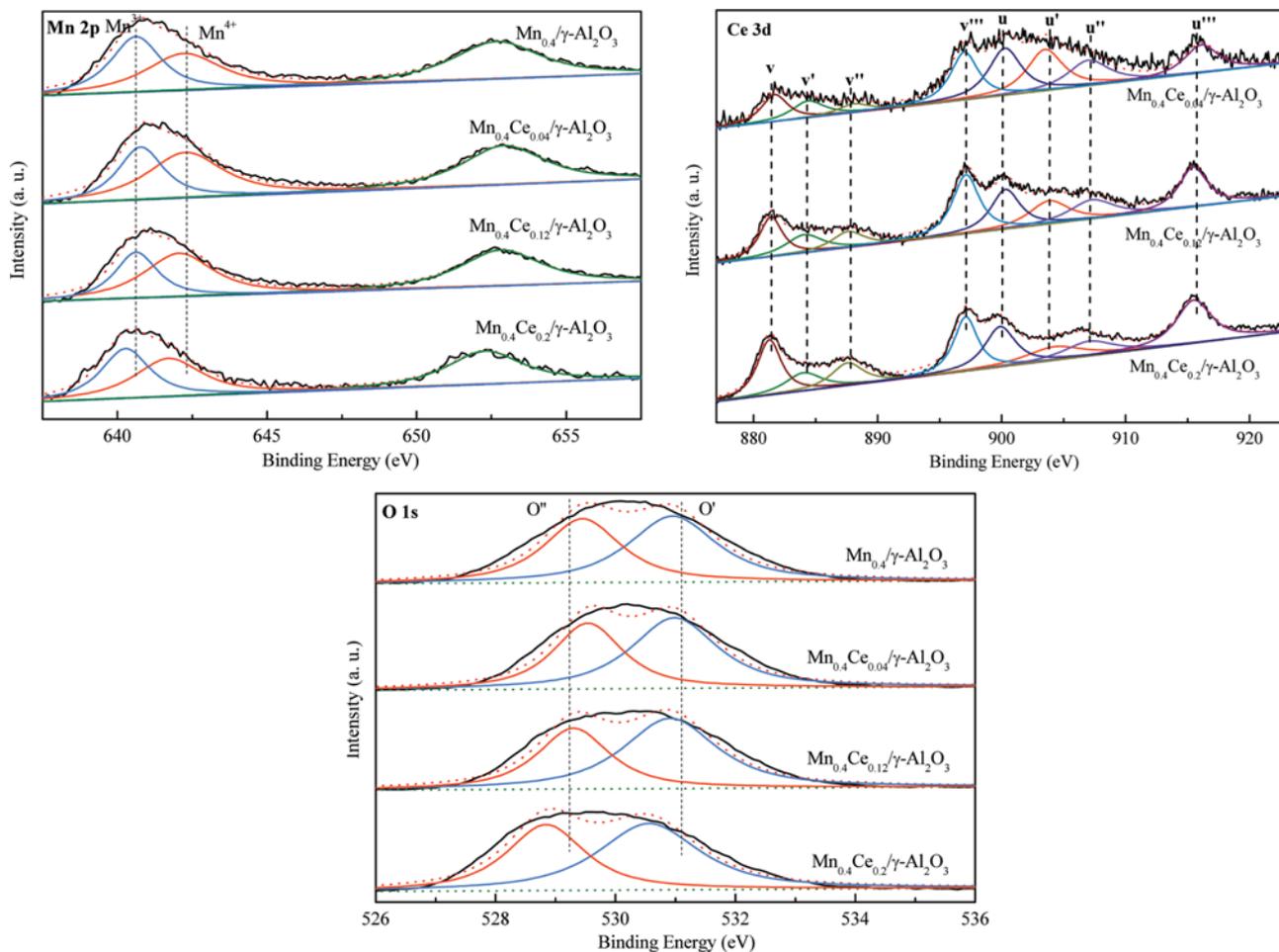
Two peaks due to Mn  $2p_{1/2}$  and Mn  $2p_{3/2}$  were observed in Mn 2p spectra. The Mn  $2p_{3/2}$  spectra could be separated into two fitting peaks around 640.5 eV and 642.2 eV, which could be assigned to  $\text{Mn}_2\text{O}_3$  and  $\text{MnO}_2$ , respectively [31]. It indicated that  $\text{Mn}^{3+}$  and  $\text{Mn}^{4+}$  co-existed on the catalyst surface. Ce 3d spectra were com-

**Table 2. The surface atomic concentration of the catalysts**

Sample	O (%)		Ce (%)		Mn (%)	
	O'	O''	Ce <sup>3+</sup>	Ce <sup>4+</sup>	Mn <sup>3+</sup>	Mn <sup>4+</sup>
$\text{Mn}_{0.4}/\gamma\text{-Al}_2\text{O}_3$	22.86	19.38	-	-	1.87	1.87
$\text{Mn}_{0.4}\text{Ce}_{0.04}/\gamma\text{-Al}_2\text{O}_3$	23.49	17.65	0.20	0.60	1.56	2.15
$\text{Mn}_{0.4}\text{Ce}_{0.12}/\gamma\text{-Al}_2\text{O}_3$	24.11	16.07	0.30	1.15	1.44	2.24
$\text{Mn}_{0.4}\text{Ce}_{0.2}/\gamma\text{-Al}_2\text{O}_3$	22.49	17.28	0.51	2.47	1.08	1.00

plicated. The peaks denoted by u', v' were assigned to  $\text{Ce}^{3+}$  and the other peaks denoted by u, u'', u''', v, v'', v''' were assigned to  $\text{Ce}^{4+}$  [32,33]. From these peaks,  $\text{CeO}_2$  was the major phase and the peaks corresponding to  $\text{Ce}^{4+}$  became stronger with the increase of Ce loading. Only one main peak was detected in O 1s spectra, which could be deconvoluted into two sub-bands. The peaks at 529.3-529.9 eV and 531.3-531.7 eV were corresponding to lattice oxygen (denoted as O'') and surface adsorbed oxygen (denoted as O'), respectively [34]. As shown in Table 2, the surface concentrations of O' and Mn<sup>4+</sup> increased after Ce addition, and the maximum values turned up in  $\text{Mn}_{0.4}\text{Ce}_{0.12}/\gamma\text{-Al}_2\text{O}_3$ .

The main reason for the inhibition of  $\text{SO}_2$  for SCR activity at low temperature is that  $\text{SO}_2$  can react with  $\text{NH}_3$  forming ammo-



**Fig. 4. XPS spectra of O 1s, Ce 3d and Mn 2p for different catalysts.**

nia sulfate to cover the catalyst surface. Combining the characterization results and catalytic activity, it can be concluded that Ce modified catalyst, especially for Mn<sub>0.4</sub>Ce<sub>0.12</sub>/γ-Al<sub>2</sub>O<sub>3</sub>, has a larger surface areas and higher active component dispersion degree, which makes more active sites exposed on the catalyst surface. For Mn<sub>0.4</sub>Ce<sub>0.12</sub>/γ-Al<sub>2</sub>O<sub>3</sub>, when the formed ammonia sulfate covers the catalyst surface the active sites remained can still play roles in SCR activity. Furthermore, XPS results show that Mn<sub>0.4</sub>Ce<sub>0.12</sub>/γ-Al<sub>2</sub>O<sub>3</sub> has

more surface adsorbed oxygen and Mn<sup>4+</sup> which plays a more important role in SCR activity. Therefore, Mn<sub>0.4</sub>Ce<sub>0.12</sub>/γ-Al<sub>2</sub>O<sub>3</sub> has a better SO<sub>2</sub> resistance.

### 2-3. Optimized Structures and Models

As shown in XRD results, MnO<sub>2</sub> and CeO<sub>2</sub> were main crystalline states on the catalyst surface. And XPS results showed that atomic concentrations of Mn<sup>4+</sup> and Ce<sup>4+</sup> were a little higher than that of Mn<sup>3+</sup> and Ce<sup>3+</sup>. Furthermore, previous studies have pointed

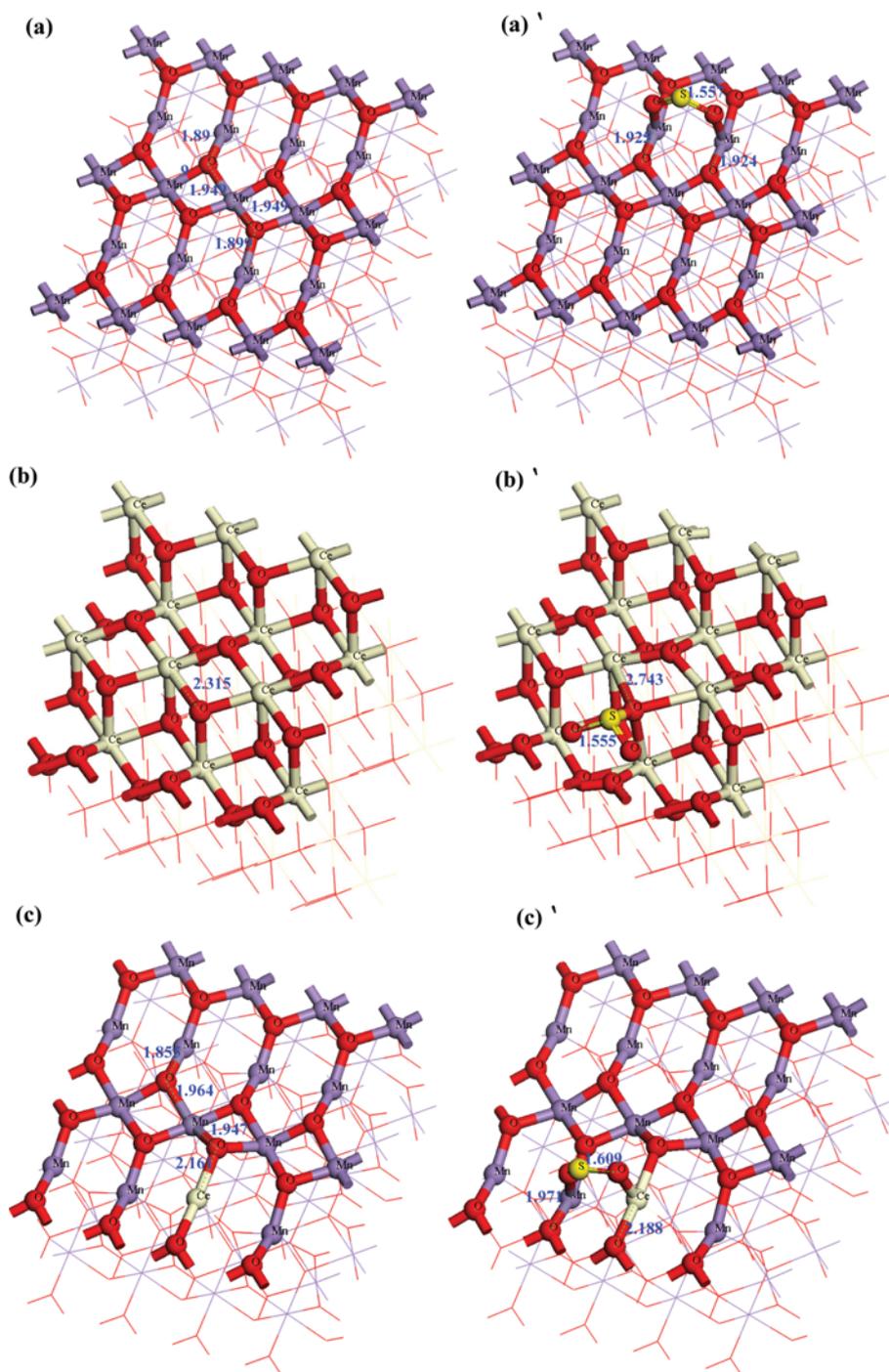


Fig. 5. The optimized structure of (a) MnO<sub>2</sub> (110), (b) CeO<sub>2</sub> (110), (c) Ce doped Mn (110) surfaces and (a)', (b)', (c)' corresponding surfaces adsorbed SO<sub>2</sub>. The red balls are oxygen, purple balls are manganese, gray balls are cerium, yellow ball is sulfur.

out that  $\text{CeO}_2$  (1 1 0) [35] and  $\text{MnO}_2$  (1 1 0) [36] play an important role during the catalytic reaction. Therefore, the  $\text{MnO}_2$  (110) and  $\text{CeO}_2$  (110) models were built. The effects of Ce doping on the adsorption of  $\text{SO}_2$  on  $\text{MnO}_2$ ,  $\text{CeO}_2$ ,  $\text{MnCe}$  (1 1 0) surface were optimized.  $\text{SO}_2$  adsorption energy on different sites was calculated. The optimized structure of  $\text{MnO}_2$  (110),  $\text{CeO}_2$  (110), Ce doped Mn (110) surfaces and the  $\text{SO}_2$  adsorption structures with highest  $\text{SO}_2$  adsorption energy are shown in Fig. 5. The other  $\text{SO}_2$  adsorption structures are shown in Fig. S1. The Mn-O and Ce-O bond length was 1.949 and 2.315 Å for  $\text{MnO}_2$  (1 1 0) and  $\text{CeO}_2$  (1 1 0) surface, respectively. These results agree with the other GGA studies [37,38]. After Ce doping, Mn-O bond with length of 1.949 Å was replaced by Ce-O with length of 2.161 Å and Mn-O bond length in the position without Ce doping changed from 1.949 to 1.964 and 1.947 Å. It suggested that Ce doping changed  $\text{MnO}_2$  (1 1 0) structure considerably at the local position, but it did not change  $\text{MnO}_2$  (1 1 0) structure much at the other position. S-O bond length for  $\text{SO}_2$  was 1.482 Å, and it increased after being adsorbed on the catalyst surface, and the Ce-O and Mn-O bonds were also changed. These results are due to the interaction between  $\text{SO}_2$  and the catalyst surface. The adsorption energy of  $\text{SO}_2$  adsorbed on  $\text{MnO}_2$ ,  $\text{CeO}_2$ ,  $\text{MnCe}$  (1 1 0) was  $-0.88$ ,  $-1.21$ ,  $-1.28$  eV, which implied that  $\text{SO}_2$  was preferably adsorbed on the Ce surrounding after Ce doping  $\text{MnO}_2$  (1 1 0). Thus, Ce doping could protect the main active component  $\text{MnO}_2$  from  $\text{SO}_2$  poisoning, resulting in a better  $\text{SO}_2$  resistance. Ji et al. [39,40] studied the effect of ceria on the sulfation of the catalyst with DRIFTS, and pointed out that ceria was able to store sulfur during catalyst exposure to  $\text{SO}_2$ . In the present work, DFT calculated results are in good agreement with these experimental results.

#### 2-4. FT-IR Analysis

FT-IR analyses were performed to investigate surface species on the catalysts after 6 h treatment with  $\text{H}_2\text{O}$  and  $\text{SO}_2$ . As shown in Fig. 6, a strong peak at  $1,640\text{ cm}^{-1}$  ascribed to symmetric bending vibration of ammonia cation  $\text{NH}_4^+$  was detected in both catalysts, which might be due to the formation of  $\text{NH}_4\text{NO}_3$  during the SCR

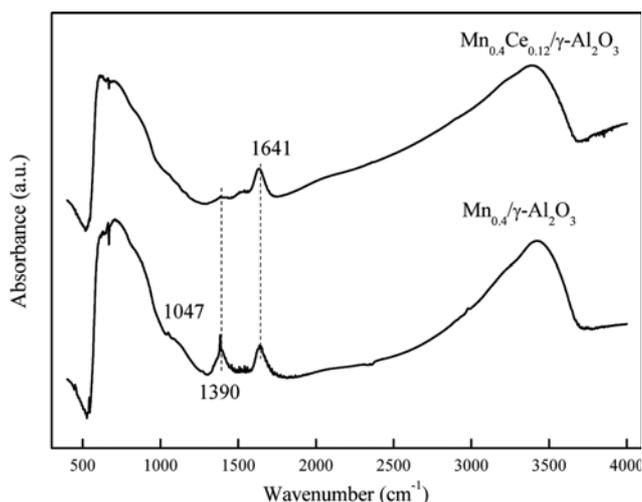


Fig. 6. FT-IR spectrum of the catalysts after 6 h treatment with  $\text{H}_2\text{O}$  and  $\text{SO}_2$ .

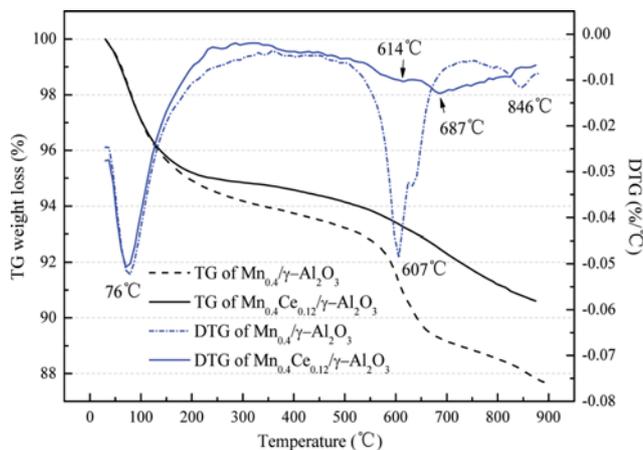


Fig. 7. TG analyses for the catalysts after 6 h treatment with  $\text{H}_2\text{O}$  and  $\text{SO}_2$ .

reaction [41,42]. Two peaks at  $1,047$  and  $1,390\text{ cm}^{-1}$  were detected in  $\text{Mn}_{0.4}/\gamma\text{-Al}_2\text{O}_3$ , which might be related to  $\text{SO}_4^{2-}$  and  $\text{NH}_4^+$  showing the existence of  $(\text{NH}_4)_2\text{SO}_4$  or  $\text{NH}_4\text{HSO}_4$  [43]. But for  $\text{Mn}_{0.4}\text{Ce}_{0.12}/\gamma\text{-Al}_2\text{O}_3$ , the peak at  $1,390\text{ cm}^{-1}$  was much weaker and the peak at  $1,047\text{ cm}^{-1}$  disappeared. Those results indicate that sulfate species could not easily accumulate on the surface of  $\text{Mn}_{0.4}\text{Ce}_{0.12}/\gamma\text{-Al}_2\text{O}_3$  during treatment with  $\text{H}_2\text{O}$  and  $\text{SO}_2$ . Previous studies reported that  $\text{SO}_2$  could react with ammonia to form ammonium sulfate which was deposited on the active sites and blocked the active channels of catalyst [13-15]. Therefore, lower formation of ammonium sulfate on the surface of  $\text{Mn}_{0.4}\text{Ce}_{0.12}/\gamma\text{-Al}_2\text{O}_3$  resulted in a better resistance to  $\text{H}_2\text{O}$  and  $\text{SO}_2$ .

#### 2-5. TG Analysis

TG analysis was used to investigate the species and stability of the sulfates on the catalysts surface. As shown in Fig. 7, the sharp peak in DTG trace at  $76^\circ\text{C}$  in both the two catalysts was attributed to the departure of water molecules and hydration. And no visible weight loss stage at  $250\text{-}350^\circ\text{C}$  corresponding to decomposition of  $(\text{NH}_4)_2\text{SO}_4$  and  $\text{NH}_4\text{HSO}_4$  [44] could be found, which indicated that ammonium sulfate could not easily form on the surface of these two catalysts. In  $\text{Mn}_{0.4}/\gamma\text{-Al}_2\text{O}_3$ , there were two other obvious peaks at  $607$  and  $846^\circ\text{C}$  which could be assigned to the decomposition of  $\text{Al}_2(\text{SO}_4)_3$  [45] and  $\text{MnSO}_4$  [11,13]. But for  $\text{Mn}_{0.4}\text{Ce}_{0.12}/\gamma\text{-Al}_2\text{O}_3$ , the peak around  $607^\circ\text{C}$  weakens remarkably and a new weak peak around  $687^\circ\text{C}$  due to  $\text{Ce}_2(\text{SO}_4)_2$  decomposition was observed [11, 46]. Furthermore, no visible peak due to sulfated  $\text{MnO}_x$  decomposition could be detected in  $\text{Mn}_{0.4}\text{Ce}_{0.12}/\gamma\text{-Al}_2\text{O}_3$ . These results indicate that Ce modification can inhibit sulfate formation on the surface of catalysts, which is in good agreement with the DFT results. Based on the above, Ce modification can change the adsorption energy of  $\text{SO}_2$  adsorbed on catalyst surface, lead to the preferential adsorption of  $\text{SO}_2$  on Ce surrounding, and inhibit sulfate formation on active component. It has been reported that the formation of sulfates, such as ammonia sulfates and metal sulfates, is the main reason for catalyst deactivation in the presence of  $\text{SO}_2$  [47,48]. Ce inhibits sulfates formation on catalyst surface especially on active component  $\text{MnO}_x$ , which can improve the  $\text{SO}_2$  resistance of catalysts, resulting in a better SCR activity in the presence of  $\text{SO}_2$ .

### 3. Conclusions

An experimental and DFT study was made to investigate the effects of Ce doped Mn<sub>0.4</sub>/γ-Al<sub>2</sub>O<sub>3</sub> on SO<sub>2</sub> resistance. DFT results show that Ce modification can change the adsorption energy of SO<sub>2</sub> adsorbed on catalyst surface, resulting in the preferential adsorption of SO<sub>2</sub> on Ce surrounding. FT-IR and TG results show that fewer sulfates can form on the catalyst surface. Therefore, Ce modification inhibiting sulfate formation on active components leads to a high NO conversion in the presence of SO<sub>2</sub>.

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### SUPPORTING INFORMATION

Additional information as noted in the text. This information is available via the Internet at <http://www.springer.com/chemistry/journal/11814>.

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## Supporting Information

### Mechanism of Ce promoting SO<sub>2</sub> resistance of MnO<sub>x</sub>/γ-Al<sub>2</sub>O<sub>3</sub>: An experimental and DFT study

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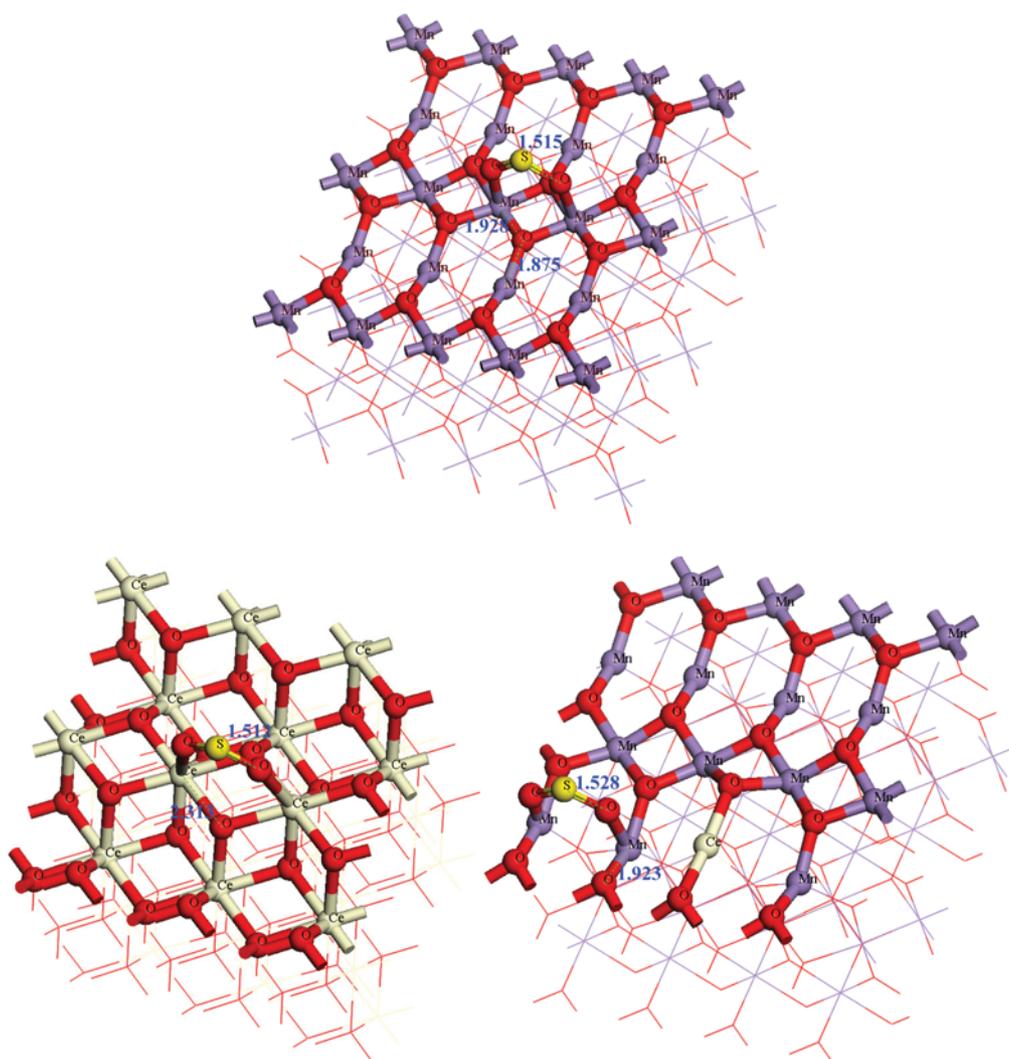


Fig. S1. The optimized structure of SO<sub>2</sub> adsorbed on (a) MnO<sub>2</sub> (110), (b) CeO<sub>2</sub> (110), (c) Ce doped Mn (110) surfaces. The red balls are oxygen, purple balls are manganese, gray balls are cerium, yellow ball is sulfur.

The adsorption energy of SO<sub>2</sub> adsorbed on MnO<sub>2</sub>, CeO<sub>2</sub>, MnCe (1 1 0) were -0.31, -0.50, -0.67 eV.