

## DISSIPATIVE STRUCTURES IN A REACTION-DIFFUSION SYSTEM

Sang Hwan KIM\* and Sang Cheol YEO

Department of Chemical Engineering, Konkuk University, Seoul 133-701, Korea

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**Abstract**—A transient analysis of reaction-diffusion equations associated with the model reaction of Prigogine and Lefever (Brusselator model), has been performed. For low system lengths and for fixed boundary conditions, steady state solutions with the low amplitude are unstable. For zero flux boundary conditions the multiplicity of symmetric solutions with the same wave number may exist and the majority of them are unstable. The diffusion of initial components induces relaxation oscillations in space for fixed as well as zero flux boundary conditions. The amplitude of the oscillations increases as the diffusion coefficient of the initial component decreases. For conditions of relaxation oscillations the spatial profiles result in single or multiple propagating fronts.

High system lengths for both zero flux and periodic boundary conditions, may give rise to a multipeak incoherent wave pattern. For periodic boundary conditions the multiplicity of waves has been observed. Numerical simulation of two-dimensional spatial structures reveals the existence of certain similarities between the one- and two-dimensional cases.

### INTRODUCTION

It is widely known that the interaction of reaction and diffusion in open systems operating far from the thermodynamic equilibrium gives rise to many interesting phenomena such as spatially homogeneous periodic solutions, nonhomogeneous periodic solutions, travelling waves, shock structures, and so forth [1-3]. Prigogine and Nicolis [4] have termed these structures arising in reaction-diffusion systems as dissipative structures. Since the classical paper by Prigogine and Nicolis in 1967 [5], the volume of literature in this field has been growing steadily. The reaction-diffusion equations coupled with appropriate kinetic expressions have been shown to serve as simple models of a number of biological phenomena and may also explain similar phenomena in many other fields.

The occurrence of multiple stable solutions for the Brusselator chemical network has been analytically predicted via the bifurcation theory and confirmed numerically by Herschkowitz-Kaufman [1] and Nicolis et al. [4]. For this model they have reported multiple stable symmetric and asymmetric steady state solutions, homogeneous periodic solutions, and travelling waves in one dimension while for a two-dimensional

geometry like a cycle they have obtained rotating waves and nonhomogeneous periodic solutions. Kubicek et al. [6] have numerically constructed a typical bifurcation diagram for this network by employing a continuation algorithm. In their study the primary bifurcation points were located analytically while the space profiles were computed numerically. The calculated steady state profiles were tested for stability and asymptotic behavior. The Brusselator chemical network has been subjected to many theoretical investigations since it exhibits many interesting phenomena and is easy to analyze because of a single homogeneous (thermodynamic) solution. In the majority of previous studies the initial components A and B are assumed to be maintained uniform throughout the system by some external mechanism. A realistic description, however, requires the inclusion of diffusion of these components. In this paper, therefore, we consider a modified Brusselator model which includes the diffusion of initial components. Here we are going to investigate the stability of computed steady state solutions via transient analysis, consider the effect of diffusion of initial components on the periodicity of solutions, study the equivalence between one- and two-dimensional geometries, and report on some numerically observed periodic solutions in one- and two-space dimensions.

\*Author to whom correspondence should be addressed.

### BRUSSELTOR MODEL IN REACTION-DIFFUSION SYSTEMS

The "Brusselator" model originally proposed by Prigogine and Lefever [7], corresponds to the following trimolecular scheme.



As mentioned earlier, in the majority of previous studies the concentrations of initial components A and B have been assumed to be maintained uniform (e.g. large excess of A and B or infinite diffusion coefficients,  $D_A \rightarrow \infty$  and  $D_B \rightarrow \infty$ ). In the present investigation, we include the diffusion of component A but treat B to be uniform. After neglecting all the reverse reactions and setting the rate constants to unity, following reaction-diffusion equations are obtained:

$$\partial A / \partial t = -A + D_A \nabla^2 A \quad (2)$$

$$\partial X / \partial t = A + X^2 Y - (B + 1)X + D_X \nabla^2 X \quad (3)$$

$$\partial Y / \partial t = BX - X^2 Y - D_Y \nabla^2 Y. \quad (4)$$

In these equations,  $\nabla^2$  is the Laplacian operator while  $D_X$  and  $D_Y$  are the diffusion coefficients for X and Y, respectively. The following boundary conditions are considered:

(a) Fixed boundary conditions

For a one dimensional system:

$$z=0, L; t>0 : X=X_0, Y=Y_0. \quad (5)$$

For a two dimensional geometry:

$$x=0, 1; y=0, 1; t>0 : X=X_0, Y=Y_0. \quad (6)$$

(b) Zero flux boundary conditions

For a one dimensional system:

$$z=0, L; t>0 : \partial X / \partial z = \partial Y / \partial z = 0. \quad (7)$$

For a two dimensional geometry:

$$x=0, 1 : \partial X / \partial x = \partial Y / \partial x = 0, \quad (8)$$

$$y=0, 1 : \partial X / \partial y = \partial Y / \partial y = 0. \quad (9)$$

(c) Periodic boundary conditions

$$X(0) = X(L), \quad \frac{\partial X}{\partial z}(0) = \frac{\partial X}{\partial z}(L), \quad (10)$$

$$Y(0) = Y(L), \quad \frac{\partial Y}{\partial z}(0) = \frac{\partial Y}{\partial z}(L). \quad (11)$$

For these boundary conditions we have considered the one-dimensional system only. Further, as is apparent from the physics of the problem this type of

boundary condition does not allow for inflow and outflow and hence we cannot consider the diffusion of component A.

### NUMERICAL METHOD OF SOLUTIONS

Eqs. (2)-(4) represent a set of coupled nonlinear parabolic partial differential equations. However Eq. (2) is separable from Eqs. (3) and (4) and can be solved independently to obtain the following steady state solution in one dimension.

$$A(z) = A_0 \frac{\cosh\left\{\frac{1}{\sqrt{D_A}}(z - L/2)\right\}}{\cosh\left\{\frac{L}{2\sqrt{D_A}}\right\}} \quad (12)$$

Eqs. (3) and (4), however, are coupled by the nonlinear source term and this necessitates its solution numerically. In our numerical calculations, we have used the Stormer-Numerov finite difference approximation for the space derivative. This method has large ( $h^4$ ,  $k^2$ ) accuracy but needs only three mesh points in space. The details of this technique with applications has been described elsewhere [8].

Following extrapolation formula has been used to evaluate the source term at time grid  $(j + 1/2)$  in the Crank-Nicholson method.

$$X^{j+1/2} = 1.5X^j - 0.5X^{j-1} \quad (13)$$

The method of solution also features automatic time step adjustment which is done on the basis of error between the predicted and the extrapolated values for the source term. For the case of periodic boundary conditions, the finite difference scheme introduces an off diagonal element in the tridiagonal structure and the fast solution method of Evans [9] has been used.

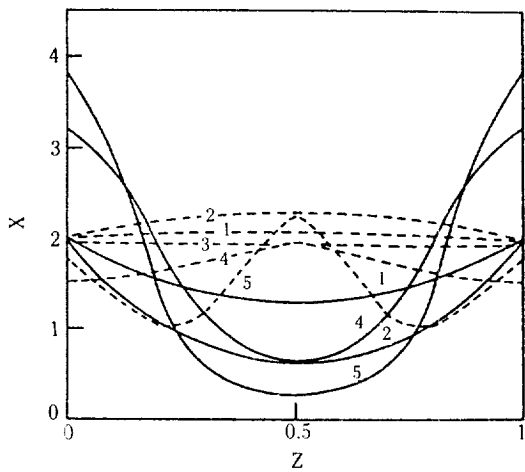
For two-dimensional problems the conventional five-point difference scheme requires solution of a banded matrix structure which is expensive. We have therefore used the ADI (Alternate direction implicit) method to calculate the space profiles in two dimensions. All the reported calculations have been performed on CDC CYBER 173 machine.

### RESULTS AND DISCUSSIONS

The following parameter values have been used in numerical calculations.

1. Steady state solutions:  $A = 2.0$ ,  $B = 4.6$ ,  $D_X = 0.0016$  and  $D_Y = 0.008$ .  $D_A$  equals 0.1 and 0.02 for fixed and zero flux boundary conditions, respectively.  $L$  is reported with each figure.

2. Periodic solutions:  $A = 2.0$ ,  $D_X = 0.008$  and  $D_Y = 0.004$ . The variation in  $L$ ,  $B$  and  $D_A$  is reported along



**Fig. 1. Spatial profiles for X. ....Steady state solution ; —transient simulation.**

Profile	1	2	3	4	5
Length	0.1	0.17	0.18	0.2	0.3

with each figure. Values of parameters other than presented above are indicated in the description of figures.

**1. Stability of steady state solutions**

The bifurcation diagrams which indicate the number and the nature of solutions of a reaction-diffusion system are usually constructed from the steady state analysis of Eqs. (2)-(4). A typical bifurcation diagram for the present system has been constructed by Hlavacek et al. [10]. The solutions obtained from the steady state analysis need not be stable and, therefore, their stability must be investigated. For this purpose we take these steady state solutions, perturb them by about 1% and study the transient behavior of the system. The solution obtained at  $t \rightarrow \infty$  is considered as the asymptotic solution. Some of the results obtained are shown in Fig. 1. The dashed lines represent the solutions calculated from the steady state analysis while the solid lines represent the corresponding stable steady state solutions obtained at  $t \rightarrow \infty$ . It can be observed from this figure that unstable symmetric solutions (dashed curves 1, 2 and 4) give rise to stable symmetric solutions with a phase shift. The unstable steady state solutions (dashed lines 1 and 2) form a part of an isolated branch on the bifurcation diagram (Fig. 4 in reference [10]) and are very close to the thermodynamic solution for fixed boundary conditions. Thus the solutions with the low amplitude (or deviations from the thermodynamic branch) seem to be unstable and the evolution process under these conditions will attract the trajectory to stable high amplitude solutions. We have further analyzed the stability of

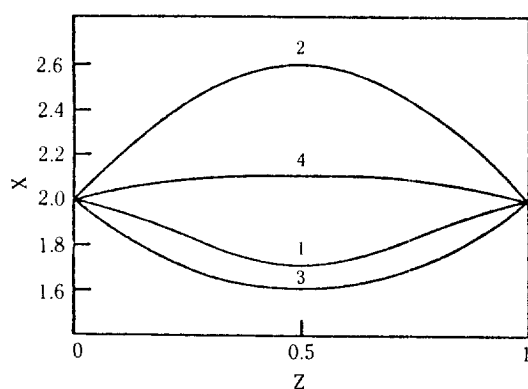
**Table 1. Comparison of exact and approximate values**

	Profile 1		Profile 2	
	X	$\bar{X}$	X	$\bar{X}$
L = 0.10	6.00	5.56	1.20	1.34
L = 0.17	0.60	0.78	3.00	2.79

these solutions by the one point collocation method [11]. The advantage of this method is it converts a system of partial differential equations to ordinary differential equations which are easier to deal with than the original partial differential equations. In this method, we place one internal point at the center of the system and write down the finite difference equations for this point. Since the boundary points are fixed, this results in a single differential equation, which can be analyzed easily to obtain approximate results. On using the Stormer-Numerov finite difference approximation, the differential equation describing the center point can be written as:

$$10 \frac{dX_m}{dt} = 12 \frac{D_x}{h^2} (X_b - 2X_m + X_b) + 10 [A_m + X_m^2 Y_m - (B + 1) X_m] \tag{14}$$

where the subscript m denotes the value of the variable at the center point while subscript b denotes the value at the boundary. Similar equation can be obtained for  $Y_m$ . Thus, we now have an initial value problem to integrate. By setting  $dX_m/dt = 0$  and  $dY_m/dt = 0$ , one can obtain the steady state values for the center point by solving the resulting nonlinear algebraic equations. On using this approach we obtained the following approximate values for the center point which are given in Table 1. In this table X indicates the value obtained by solving the full partial differential equations while  $\bar{X}$  denotes the value obtained from the one point collocation. The agreement is satisfactory and one can use this information as the first approximation. It was noticed earlier that low amplitude solutions are unstable for fixed boundary conditions. However, they have been found to be stable for zero flux boundary conditions (dashed line 3). For zero flux boundary conditions with  $L = 0.2$  Hlavacek et al. [10] have reported seven steady state profiles. Three of these profiles are symmetric with two solutions having the same wave number but different amplitudes. One of these solutions is unstable (profile 4) and the stable solution is observed to be a symmetric solution with a phase shift. It, therefore, appears that steady solutions with the same wave number but different amplitudes may



**Fig. 2. Periodic solution profile for X.**

$L = 0.4$ ,  $B = 5.4$ ,  $D_A = 0.1$ .

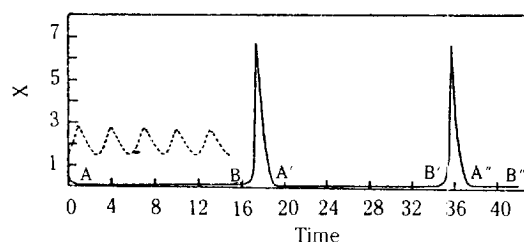
Profile	1	2	3	4
Time	11.80	12.72	13.92	15.15

not be stable at low system lengths. Profile 5, which represents a high wave number (wave number equal to three) solution for zero flux boundary conditions is also unstable and the steady solution at  $t \rightarrow \infty$  has been found to have a wave number of one.

## 2. Periodic solutions in one dimension

Depending upon the values of the kinetic and diffusion constants and the system size  $L$ , the solution bifurcating from the thermodynamic branch could either be a stable steady state or a periodic solution. Such periodic solutions may give rise to concentration waves. Pismen [12] in describing the bifurcating waves has proposed that in a one-dimensional system, depending upon initial conditions, the periodic solution may either be a propagating wave in an infinite system or a standing wave for a finite system, an ordered combination of standing waves or an incoherent pattern. Nicolis et al. [3] have analytically predicted and numerically observed the existence of standing and travelling waves for the Brusselator model.

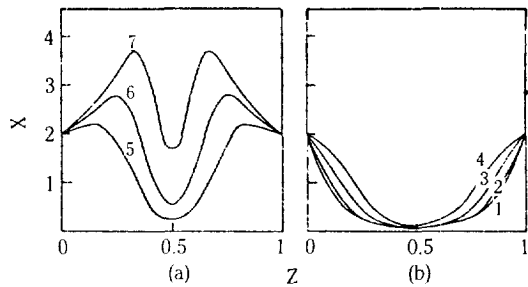
These general results obtained from the bifurcation theory may not be applicable when diffusion of initial components is also considered. Since trivial solutions ( $X_0 = A$  and  $Y_0 = B/A$ ) for the present case do not exist, it also excludes the possibility of homogeneous periodic solutions. In such a case, the first bifurcating solution, therefore, is space dependent. This solution is symmetrical and represents a standing wave. For the chosen parameters ( $A = 2.0$ ,  $B = 5.8$ ,  $D_X = 0.008$ ) the solution at low bifurcation lengths ( $L$  up to 0.6) was always symmetrical for fixed boundary conditions. Various initial non-uniform profiles were tested to see whether asymmetric solutions exist. However, in each



**Fig. 3. Oscillations of the center point.**

$L = 0.6$ ,  $B = 5.4$ ,  $\cdots D_A \rightarrow \infty$ ,  $- D_A = 0.02$ .

case, after an initial transient period the solution always evolved to a symmetric standing wave. A typical solution is shown in Fig. 2. An interesting observation was made while studying the effect of diffusion of component A on periodic solutions. It was observed that the diffusion of component A alters the period as well as the nature of oscillations. A plot of oscillations at the center point of the system is shown in Fig. 3. For the sake of comparison, the case with constant A ( $D_A \rightarrow \infty$ ) is also shown on the same figure. It is observed from this figure that when  $D_A \rightarrow \infty$ , the oscillations are fairly regular. However, with the diffusion of component A these regular oscillations change to a period of fairly low and uniform concentration of X followed by a steep spike. The period elapsed between two successive spikes is also the same. This effect seems to be quite similar to the concentration oscillation observed for the Belousov-Zhabotinsky reaction [13]. It, therefore, appears that the nonuniform distribution of component A gives rise to multiple time scales in the system. During the period A-B or A'-B' in Fig. 3, the rate of change of the component X is very low and the system appears to be almost quiescent. This period of uniformity is followed by a period of rapid transformations which involves steep time gradients. Such type of phenomena has been termed as relaxation oscillations. Herschkowitz-Kaufman and Nicolis [14] have also reported relaxation oscillations for this model but they have analyzed only fixed boundary conditions. The transient space profiles during the period B'-A'' are shown in Fig. 4(a) while Fig. 4(b) depicts the transient profiles in the region A'-B'. These figures reveal that during the short time scale propagating fronts are observed which move from the boundary towards the center, collide and ultimately change to a standing wave pattern, which is carried into the quiescent region A''-B'' as shown in Fig. 4(b). In order to explain the existence of the propagating fronts in the short time interval, we can make use of the theory of propagation of fronts and discontinuity by Ortoleva and Ross [15]. According to this theory propagating fronts are observed for systems with kinetics on



**Fig. 4. Propagating fronts for fixed boundary conditions.**  
 $L = 0.6, B = 5.4, D_A = 0.02$ .  
Profile 1 2 3 4 5 6 7  
Time 20.25 21.66 25.56 29.40 35.76 36.06 36.25

multiple time scales and possessing multiple homogeneous stationary states. Since these phenomena are observed with nonuniform distribution of component A, it is suspected that diffusion of A may cause the introduction of multiple pseudo stationary states although for the Brusselator model with constant A only one stationary homogeneous state exists. In order to explain the existence of multiple pseudo stationary homogeneous solutions for the Brusselator model, we make use of Fig. 3 and attempt the following explanation. From this figure it can be inferred that in the period A-B the concentration at the center point almost approaches zero. Since for a long time the concentration profiles remain flat in the central portion of the system, the effect of diffusion here can be neglected.

In this case our equations become

$$dX/dt = A + X^2Y - (B+1)X \tag{15}$$

and

$$dY/dt = BX - X^2Y. \tag{16}$$

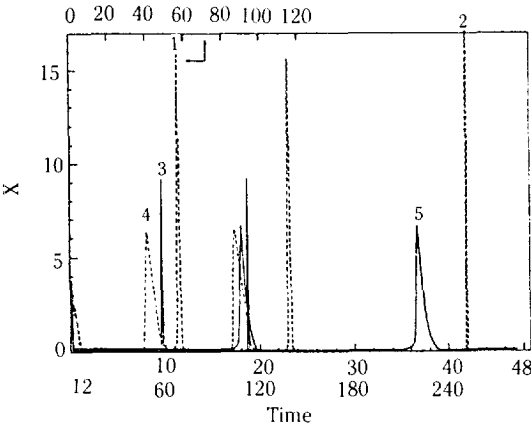
In order to obtain the homogeneous solutions we set  $dX/dt = dY/dt = 0$  and solve the resulting algebraic equations which are given as

$$A + X^2Y - (B+1)X = 0 \tag{17}$$

and

$$BX - X^2Y = 0. \tag{18}$$

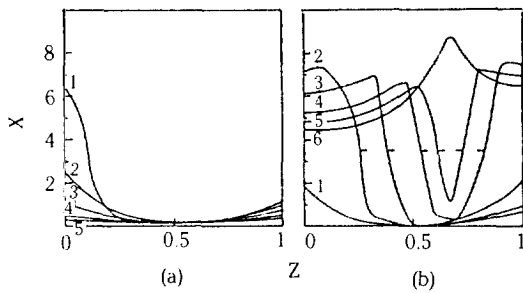
If  $X \neq 0$ , to satisfy Eq. (17),  $A \cong 0$ . If we take a value of  $D_A \cong 0.002$  and  $L = 0.4$ , A at the center  $\cong 0.02$ . These  $X \cong 0$  satisfies Eq. (17). Now from Eq. (18) one can obtain  $X = 0$  and  $X = B/Y$  as the solutions. The root  $X = B/Y$  further shows that since B is constant, an increase in X is accompanied by a corresponding decrease in Y which is observed in the solution of full partial differential equations for this case. These multiple pseudo-



**Fig. 5. Oscillations of the center point. .... Zero flux boundary conditions; — fixed boundary conditions.**

Profile	1	2	3	4	5
L	0.4	0.4	1.0	0.6	0.6
B	5.4	5.4	5.4	5.4	5.4
$D_A$	0.001	0.0002	0.02	0.02	0.02

stationary states probably give rise to the propagating fronts which are shown in Fig. 4(b). To investigate the effect of diffusion of A on the relaxation oscillations,  $D_A$  was changed from 0.1 to 0.0002 for zero flux as well as fixed boundary conditions and the observed oscillations have been reported in Fig. 5. The dashed lines in this figure show oscillations for zero flux boundary conditions while the solid lines are for fixed boundary conditions. This plot reveals that for the same parameters, the oscillation period for fixed boundary conditions is almost twice than that for zero flux boundary conditions. Also, the comparison of profiles 1 and 2 indicates that as  $D_A$  decreases, the period of oscillations as well as the amplitude of oscillations increases. However, in all cases, the nature of the space profiles remains the same. It was also noticed that for the chosen parameters fixed boundary conditions always resulted in symmetrical structures while for zero flux boundary conditions asymmetric space profiles are possible. A typical transient profile for zero flux boundary conditions, illustrating the development of a propagating front from a standing wave is shown in Fig. 6. Another observation made in this study indicates that when  $D_A \rightarrow \infty$ , for the systems of low size all space points fall on the same limit cycle. However, when  $D_A$  assumes low values (say 0.002), two distinct but interwoven limit cycles are observed for the center and the boundary points. If we extrapolate the above mentioned arguments, it can be said that when  $D_A$  assumes very low values, the development of shock

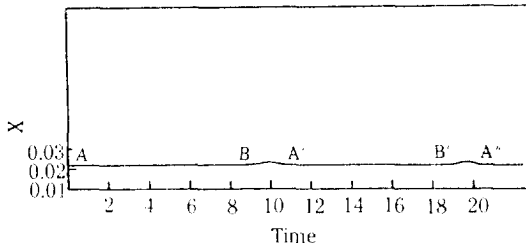


**Fig. 6. Propagating fronts for zero flux boundary conditions.**

$L = 0.6$ ,  $B = 5.4$ ,  $D_A = 0.02$ .

(a) Profile 1 2 3 4 5  
Time 0.1 4.6 5.82 6.03 6.13

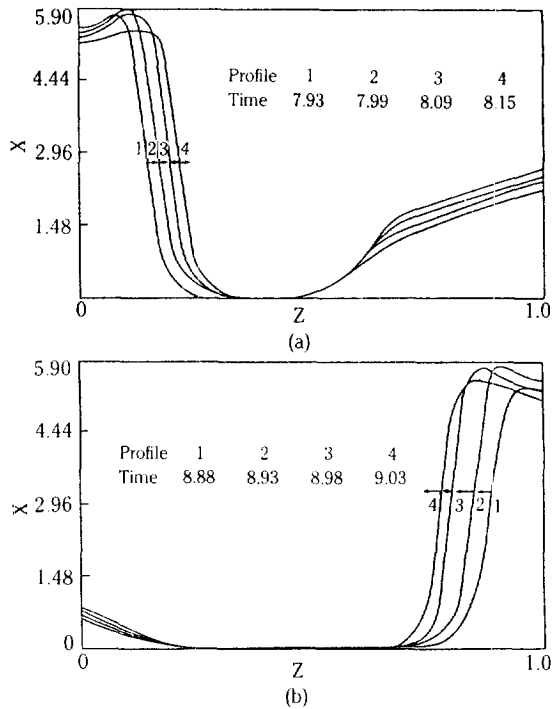
(b) Profile 1 2 3 4 5 6  
Time 7.35 7.62 7.82 8.02 8.07 8.21



**Fig. 7. Oscillations of the center point.**

$A = 1.7$ ,  $B = 4.28$ ,  $L = 1.0$ ,  $D_X = 0.01$ ,  $D_Y = 0.0$ ,  $D_A = 0.02$ .

structures from seemingly quiescent medium might be observed. As mentioned earlier, a nonuniform distribution of the component A causes simultaneous propagation of fronts either boundaries towards the center. We have also calculated for a different set of parameters and initial conditions, a different type of relaxation oscillations where the amplitude of oscillations for the center point is quite small as shown in Fig. 7. For this case we observed a single propagating front moving from left to the center for a short period during the phase A-B, which is shown in Fig. 8(a), while an identical front moves from the right to the center during the phase B'-A'' for another short interval as depicted in Fig. 8(b). These fronts, however, do not reach the center but disappear in between. It was also noticed that an increase in the system dimension or a decrease in diffusion coefficients increased the phase difference between various spatial points. As can be expected, a nonuniform distribution of the component A affects stability and the reported bifurcation analysis of the Brusselator model by Herschkowitz-Kaufman [1] is not applicable here. The bifurcation theory for

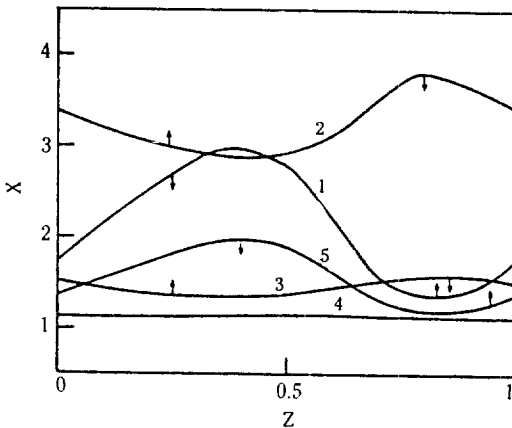


**Fig. 8. Single propagating front for zero flux boundary conditions.**

Parameters same as for Fig. 7.

$D_A \rightarrow \infty$  predicts a homogeneous stable solution for the parameters  $A = 2.0$ ,  $B = 5.4$ ,  $L = 0.4$ ,  $D_X = 0.008$  and  $D_Y = 0.004$  for constant boundary conditions. However, when  $D_A = 0.1$ , the same parameters yield a periodic solution with standing wave characteristics. Our one point collocation approach did show this stability change and the solution of the corresponding ordinary differential equations showed oscillations for the center point.

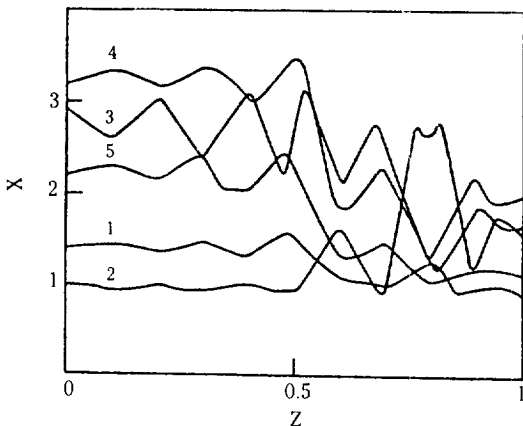
Our numerical experiments for the periodic boundary conditions resulted in a travelling wave and multiplicity of standing waves. Fig. 9 illustrates a typical two standing waves pattern. It can be easily observed that each is a nonlinear wave and the two waves are out of phase with each other. The duration for which each wave is observed during a period, however, is not the same. For high values of  $L$  or low diffusion coefficients, we have observed periodic solutions of increasing complexity. A typical periodic solution is shown in Fig. 10 which describes a multipeak standing wave with incoherent pattern. In general, it has been noticed that multipeak periodic solutions are possible only at high system lengths. Also the periodic solutions for zero flux or periodic boundary conditions at high system lengths have similar characteristics.



**Fig. 9. Two standing wave patterns for periodic boundary conditions.**

$A = 2.0$ ,  $B = 5.4$ ,  $D_X = 0.008$ ,  $D_Y = 0.004$ ,  $L = 2.0$ .

Profile	1	2	3	4	5
Time	2.74	3.44	4.78	5.58	6.24



**Fig. 10. Incoherent wave pattern for zero flux boundary conditions.**

$A = 1.7$ ,  $B = 4.28$ ,  $L = 100$ ,  $D_X = 1.0$ ,  $D_Y = 0.0$ .

Profile	1	2	3	4	5
Time	0.1	1.2	2.57	2.82	3.48

### 3. Dissipative structures in two-dimensions (rectangular geometry)

The theory of linear stability analysis indicates that the bifurcation from the homogeneous stable solution takes place when at least one eigenvalue of the matrix  $[A - \lambda_n D]$  has a positive real part. The matrix  $A$  for the Brusselator model can be expressed as

$$A \equiv \begin{pmatrix} \frac{\partial F}{\partial X} & \frac{\partial F}{\partial Y} \\ \frac{\partial G}{\partial X} & \frac{\partial G}{\partial Y} \end{pmatrix} \quad (19)$$

where  $F$  and  $G$  are given as

$$F = A + X^2 Y - (B + 1)X \quad \text{and} \quad G = BX - X^2 Y. \quad (20)$$

All the required derivatives are evaluated at  $X_0$  and  $Y_0$  which are the solutions to  $F = 0$ ,  $G = 0$ . The matrix  $D$  is a diagonal matrix of the diffusion coefficients and  $\lambda_n$  are the eigenvalues of the following scalar equation [16]:

$$\nabla^2 X + \lambda X = 0 \quad \text{for } X \in \Omega. \quad (21)$$

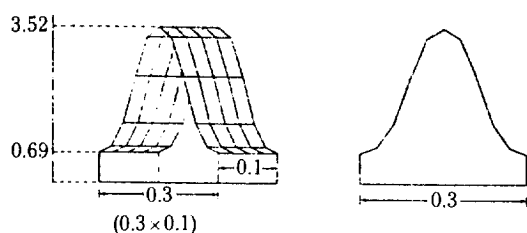
For the one-dimensional model  $\lambda_n$  are given by  $n^2 \pi^2 / L^2$  for both zero flux as well as fixed boundary conditions where  $n = 0, 1, 2, \dots$  and  $n = 1, 2, \dots$  for zero flux and fixed boundary conditions, respectively. For the two-dimensional rectangular geometry  $\lambda_n$  are given by

$$\lambda_n = \pi^2 (m^2 + \delta^2 n^2) / L^2 \quad (22)$$

where  $\delta$  is the aspect ratio (=height/length) and  $m$  and  $n$  have the same values as  $n$  for the one-dimensional system. From the analysis mentioned above, one clearly observes that when  $\delta = 1$  and  $m = 0$ , the bifurcation pattern of one- and two-dimensional systems is the same. In other words, the parameter values for which the one-dimensional system shows bifurcation will also cause the bifurcation for the two-dimensional case. In our numerical calculations we have, therefore, used the same parameters as those used for one-dimensional calculations. One can further observe that if in the reaction-diffusion equation

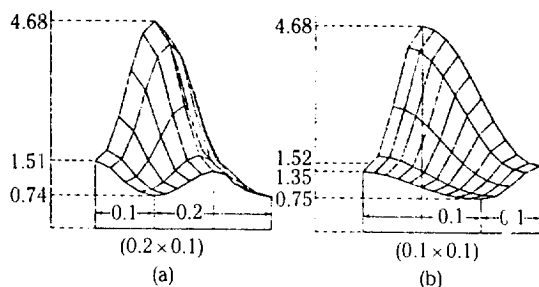
$$\frac{\partial X}{\partial t} = F + D_x \left( \frac{\partial^2 X}{\partial x^2} + \frac{\partial^2 X}{\partial y^2} \right) \quad (23)$$

one of the second derivatives is set to zero, the system will be reduced to the one-dimensional description. In such a case, all one-dimensional steady state solutions will be the solutions in two dimensions with no gradient along  $x$  and  $y$  direction depending upon which ever second derivative is set to zero. We have tested this observation for the zero flux boundary condition. For  $L = 0.3$  and  $\delta = 1$ , we have calculated a steady state solution in one dimension and constructed a two-dimensional solution starting from it. The calculated steady state solution and the corresponding one-dimensional solution are shown in Fig. 11. For this case we also calculated some additional steady state solutions in two dimensions by knowing the one-dimensional profiles. Variation of the aspect ratio does not affect the qualitative as well as quantitative nature of these solutions as is apparent from the analysis. It should, however, be noticed here that the above mentioned analysis applies only to the case when the component  $A$  is assumed to be constant ( $D_A \rightarrow \infty$ ). When  $A$  is distributed nonuniformly, the resulting steady state



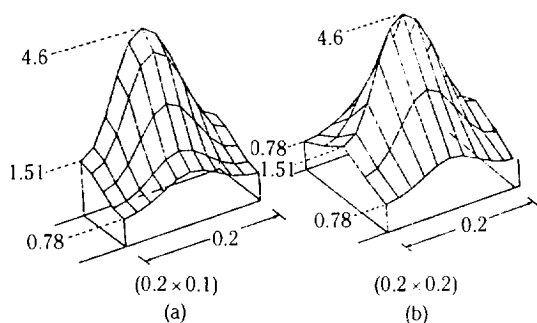
**Fig. 11. Two dimensional analogue of one dimensional space structure.**

$L = (0.3 \times 0.1)$ .



**Fig. 12. Symmetric and asymmetric space structures in two dimensions.**

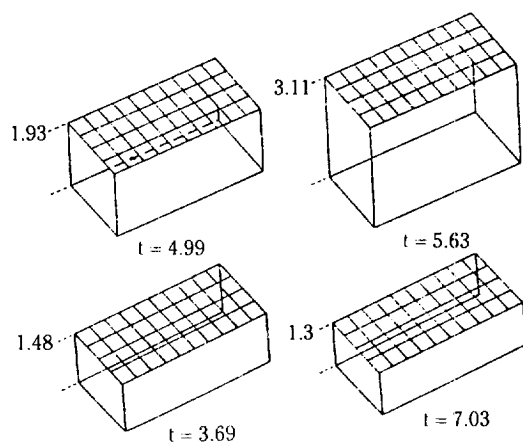
(a)  $L = (0.2 \times 0.1)$ ; (b)  $L = (0.1 \times 0.1)$ .



**Fig. 13. Composing solutions in two dimensions.**

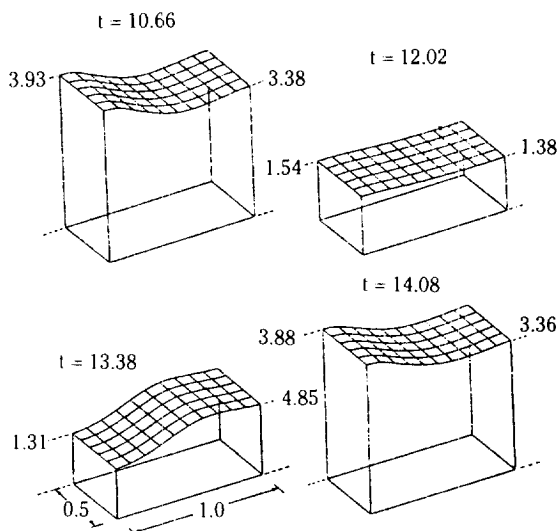
(a)  $L = (0.2 \times 0.1)$ ; (b)  $L = (0.2 \times 0.2)$ .

solutions are qualitatively similar but quantitatively different. The two-dimensional solutions obtained from the one-dimensional profiles are termed as 1-D analogues. Apart from these 1-D analogues we have also calculated some other symmetric as well as asymmetric solutions. Some of these are reported in Fig. 12. The reported asymmetric solutions are found to be mirror image of one another. Further, by using the symmetric properties, we can obtain four steady-states from one solution. Another interesting property observed for zero flux boundary conditions was that of composing solutions for systems of high size knowing the steady state solutions for the low size. A typical



**Fig. 14. Two dimensional analogue of homogeneous periodic solution.**

$L = (0.2 \times 0.1)$ .

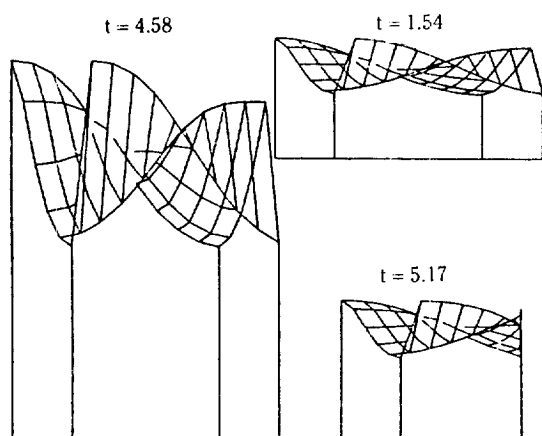


**Fig. 15. Two dimensional analogue of a standing wave.**

$L = (1.0 \times 0.5)$ .

result is shown in Fig. 13. Such composing of solutions in one dimension has already been discussed by Kubicek et al. [6]. As mentioned earlier since all one-dimensional solutions are solutions in two dimensions under certain conditions, we could calculate the analogue of one-dimensional periodic solutions also in two dimensions. The two-dimensional analogue of a homogeneous periodic solution is a plane which goes up and down and is shown in Fig. 14 while the analogue of a standing wave is a vibrating plane which moves up and down as shown in Fig. 15. The calcula-





**Fig. 16. Antisymmetric periodic structures.**  
 $L = (1.6 \times 1.0)$ .

tions also showed that the period of oscillation for the one- and two-dimensional cases is the same. Another interesting property observed for the periodic solutions for high values of  $L (= 1.6 \times 1.0)$  and for zero flux boundary conditions was antisymmetry of the periodic structure about the central plane. Our calculations showed that the structure of the solution in the  $XY$  plane is diametrically opposite to that about the plane  $Y = Y/2$ . In other words, if we bisect the solution at the center parallel to  $X$  axis and rotate one part by  $\pi$ , the resulting structure will be exactly equivalent to the remaining portion. A typical periodic solution is shown in Fig. 16 which illustrates this point.

## CONCLUSIONS

As noticed earlier all solution profiles obtained by the steady state analysis are not stable and a transient approach is required to calculate the asymptotic properties. It is observed that low amplitude (or small deviations from the thermodynamic branch) solutions are not stable for fixed boundary conditions while same wave number multiple solutions with different amplitudes are unstable for zero flux boundary conditions. A non-uniform distribution of the component  $A$  alters the bifurcation pattern and the homogeneous stable solution gives rise to a periodic solution. Also, since diffusion of the component  $A$  does not admit trivial solution for the Brusselator model, the primary bifurcating periodic solution itself is space-dependent. It appears that an inclusion of non-uniform  $A$  can result in multiple time scales in the system and relaxation type of oscillations occur. It has been shown that propagating fronts observed in this case probably oc-

cur because of multiplicity of homogeneous solutions. Low diffusion coefficients cause high wave number periodic solutions which are of incoherent pattern. The equivalence of one- and two-dimensional structures can be explained on the basis of lateral uniformity in either directions. It is also noticed that additional interesting phenomena could be observed as the dimension of the system increases.

## NOMENCLATURE

- $A$  : component and concentration of  $A$
- $A_0$  : constant in Eq. (12)
- $B$  : component and concentration of  $B$
- $D$  : matrix of diffusion coefficients
- $D_A, D_B, D_X, D_Y$  : diffusion coefficients of components  $A, B, X$  and  $Y$ , respectively
- $E$  : component and concentration of  $E$
- $F, G$  : nonlinear source terms defined in Eq. (20)
- $h, k$  : uniform mesh intervals in the space and the time, respectively
- $L$  : length of the system size
- $m, n$  : wave numbers in two dimensions
- $t$  : time
- $x$  : space coordinate
- $X$  : component and concentration of  $X$
- $y$  : space coordinate
- $Y$  : component and concentration of  $Y$
- $z$  : space coordinate

## Greek Letters

- $\delta$  : aspect ratio (= height/length)
- $\nabla^2$  : Laplacian operator
- $\lambda$  : eigenvalues
- $\Omega$  : boundary in two dimensions

## Superscripts

- $j$  : time level
- : concentration values obtained from one point collocation in Table 1

## Subscripts

- $A$  : component  $A$
- $b$  : boundary values in Eq. (14)
- $B$  : component  $B$
- $m$  : center point in Eq. (14)
- $o$  : thermodynamic solutions
- $X$  : component  $X$
- $Y$  : component  $Y$

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